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Process Evaluations and Simulations of CO₂ Capture from Steel Plant Flue Gases

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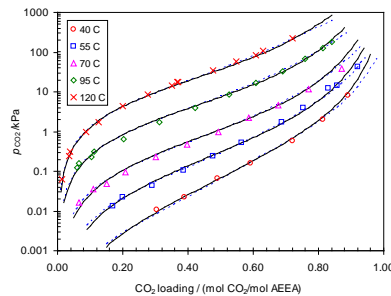
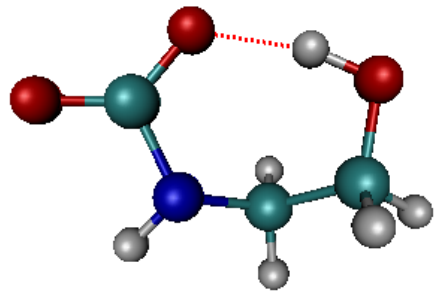
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Outline

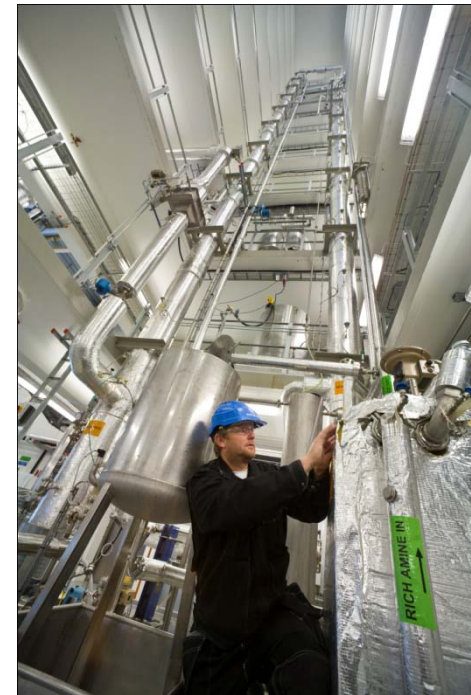
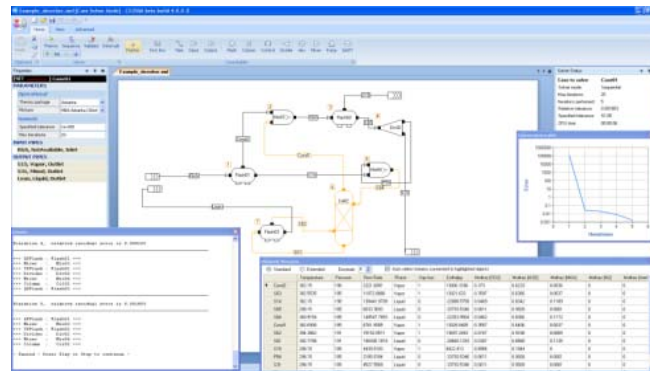
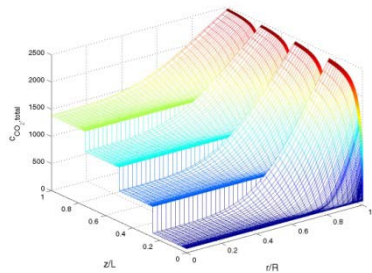
- SINTEF: Who we are
- Project objectives
- General process design and basis for simulation
 - CO₂SIM simulation software
- Second Pass simulations (separate absorbers, combined desorbers at power plant)
 - Conventional MEA plant
 - Energy saving solvent and process configuration
- CO₂ removal from an Oxygen blast furnace (OBF) stream
- Summary and conclusions

SINTEF CO₂ capture group

- The CO₂ capture group at SINTEF/NTNU is one of the worlds largest research groups within absorption technology
- Laboratories and equipment for solvent characterization from bench to pilot scale
- In house molecular simulation models, thermodynamic models and complete process simulator (CO₂SIM)



People:
CO₂ capture processes
20 researchers
NTNU Department of
Chemical Engineering
18 PhD students and
post doc



Project description

The overall project is headed by Swerea Mefos for IEA GHG,
"Techno-Economic Assessment of Carbon capture from an Integrated Steel plant"

SINTEF was to perform detailed simulations of solvent based CO₂ capture processes on various flue gases present in a conventional steel plant as well as oxygen blast furnace (OBF) gas composition.

Previously we have worked with simulation of blast furnace gases in the ULCOOS project:

- Tobiesen, F.A., Svendsen, H.F. and Mejdell, T, "Modeling of Blast Furnace CO₂ Capture Using Amine Absorbents", *Ind. Eng. Chem. Res.*, 2007, 46, 7811-7819.
- Mejdell, T., Tobiesen, A., Svendsen, H., CO₂ Capture with Chemical Absorption, ULCOOS report nr 515960: 2006.
- Mejdell and Tobiesen, CO₂ Scrubbing with Amines, UCLCOOS: SP6 2006, Trollfjord, Norway

Objective: Establish energy requirements and equipment sizing for a solvent based CO₂ capture process

1. Working on various flue gases present in an integrated steel plant
2. OBF flue gases

Input:

- Various flue gas streams present in a conventional steel plant, provided by Swerea Mefos

Investigation

- Establish energy requirements and equipment sizing
- Evaluate the concept of single absorbers for the *Steam generation, Hot stove + Coke, Lime Production* flue gases combined with solvent transport to common desorber site (second pass)
 - Evaluate CO₂ recovery of 85, 90 and 95% from the different streams to remove 75% CO₂ total
- Simulate oxygen blast furnace flue gas separation

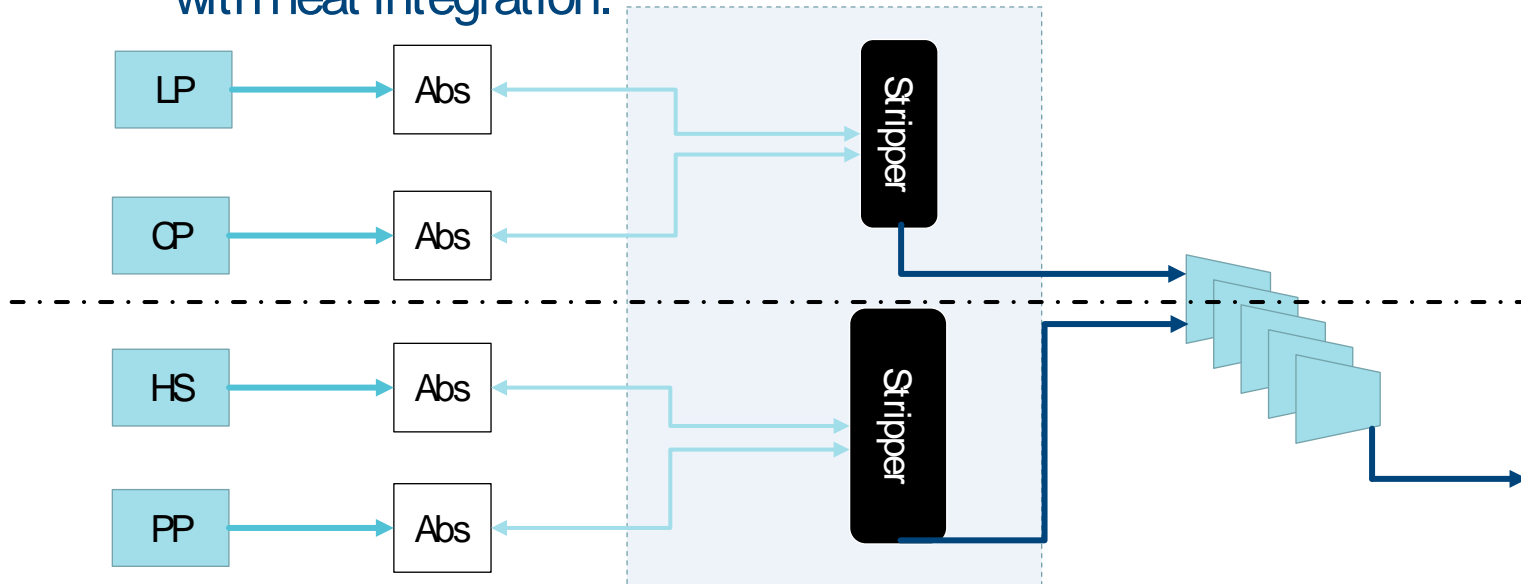
Flue gas qualities

Flue gas:		Lime Production	Coke Production	Sinter Plant	Hot Stoves	Reheating furnace	Steam Gen.
Case abbrev.		LP	CP	SP	HS	RF	PP
CO2	%	19.8	14.7	4.9	27.3	5.0	27.4
N2	%	60.0	69.5	72.0	65.6	71.3	66.1
O2	%	7.6	5.0	14.8	0.8	5.9	0.7
H2O	%	12.7	10.8	7.5	6.3	17.8	5.8
Temp	oC	120	250	120	270	500	120
Pressure	bar abs	1.08	1.08	1.08	1.08	1.08	1.08
NOX	ppmv	15.0	150.0	100.0	37.0	247.0	50.0
SOX	ppmv	3.6	21.3	106.0	18.0	5.0	14.0
CO2-flow	t/yr	298,341	771,130	1,075,557	1,660,318	230,783	3,871,852
Sum CO2 all streams	t/yr	7,907,980					

- Combination of the PP+HS and CP+LP streams into common desorbers because the streams have a similar CO₂ level.
- Power Plant/ Hot Stoves and Coke and Lime Production flue streams have high CO₂ content (slightly higher than conventional coal derived flue gas)
- Very low O₂ level of the PPHS case, CPLP similar to conventional coal case
- SO_x and NO_x for solvent degradation
 - Both NO₂ and SO₂ seem ok and manageable (similar to coal flue gas)

Second pass

- Focus primarily on the four main process streams
 - Because of distance between process streams and cost of ducting etc, we chose an option to have single absorbers for each gas at the process area and pump the solvent to a common solvent regeneration unit (desorber) next to the steam boiler, first with standard MEA
 - Test advanced energy saving solvents including process configurations with heat integration.



Simulation approach

- Set-up of simulation case in CO₂SIM
- Definition of a near optimal case, based on the CO₂ input level, characterized with a given lean loading, liquid circulation rate and reboiler duty
- Absorber and desorber dimensioning based upon the Sulpak software from the packing vendor Sulzer, using gas and liquid properties from CO₂SIM as input.
- Optimization study using routines built in CO₂SIM
 - Varying lean loading and observe the impact on reboiler duty and process utilities (cooling water and electricity for pumps and blower).

Sulpak Tower dimensioning
(diameter):

Screenshot of the SULPAK 3.1 - MefosPPHS.pak software interface showing the dimensioning of two absorption beds.

Bed 1: PP absorber

Packing							Results	
diam [m]	Packing-Type	Material	NTS	NTSM exp.	hgt [m]		hl [%]	Δp [mbar]
11.8	M2X	1.0330 (DIN)		1.5	15.249		8.4	25.60

Flows							Results			
G [kg/h]	L	ρ _G [kg/m ³]	ρ _L [mN/m]	σ	η _L [cP]	η _G	cap [%]	F-F [Pa ^{0.5}]	liq load [m ³ /m ² h]	Δp/Δz [mbar/m]
1166890	6398000	1.2	1100.0	50.0	2.23	0.018	74.3	2.95	58.00	1.679
1166890	6398000	1.2	1100.0	50.0	2.23	0.018	74.3	2.95	58.00	1.679

Text: PP absorber

Bed 2: HS absorber

Packing							Results	
diam [m]	Packing-Type	Material	NTS	NTSM exp.	hgt [m]		hl [%]	Δp [mbar]
7.4	M2X	1.0330 (DIN)		1.5	15.249		8.4	25.71

Flows							Results			
G [kg/h]	L	ρ _G [kg/m ³]	ρ _L [mN/m]	σ	η _L [cP]	η _G	cap [%]	F-F [Pa ^{0.5}]	liq load [m ³ /m ² h]	Δp/Δz [mbar/m]
501087	2744000	1.2	1100.0	50.0	2.23	0.018	74.4	2.95	58.00	1.686
501087	2744000	1.2	1100.0	50.0	2.23	0.018	74.4	2.95	58.00	1.686

Text: HS absorber

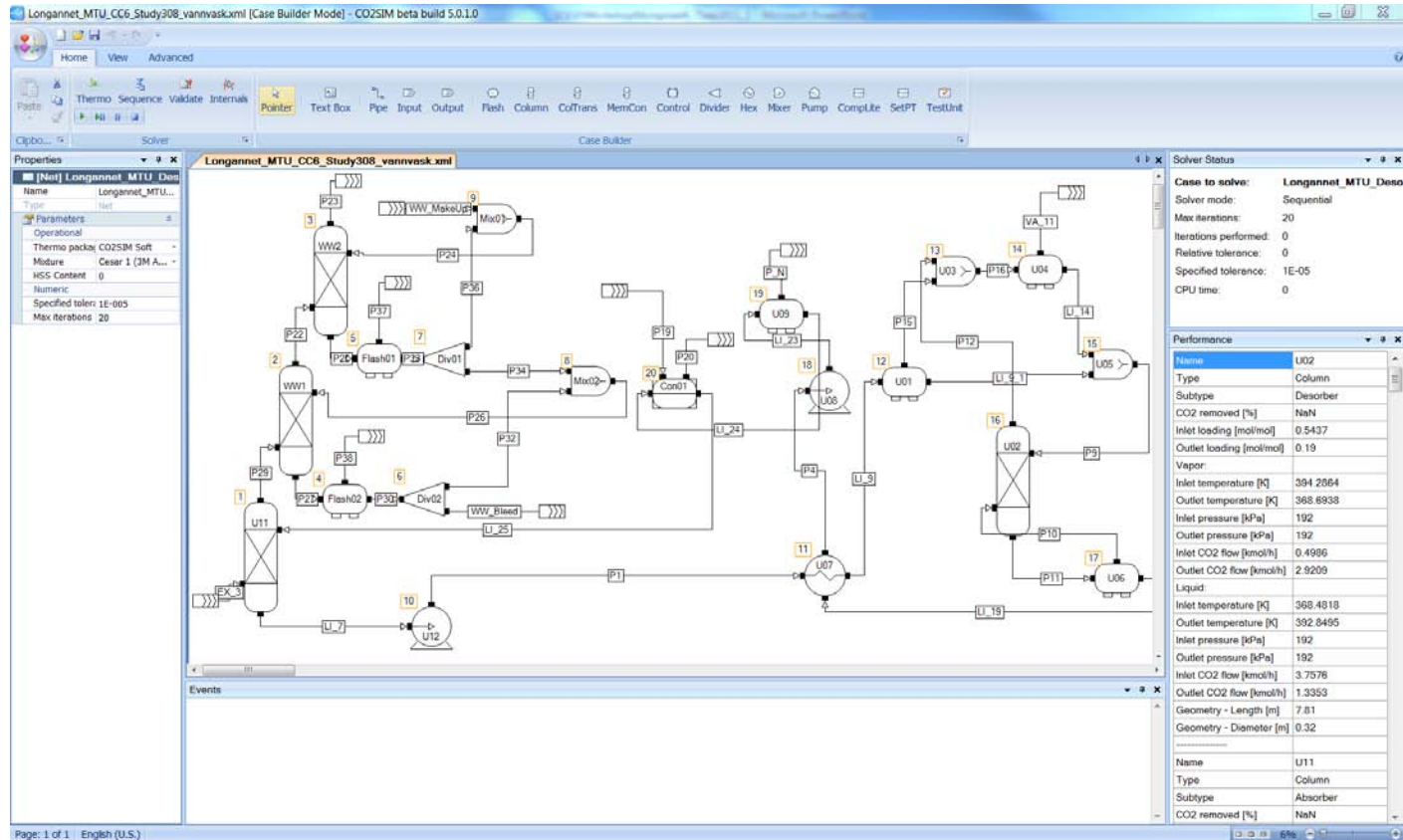
Total beds: 3

Column data: p top [mbar], Δp pack. [mbar], 76.534

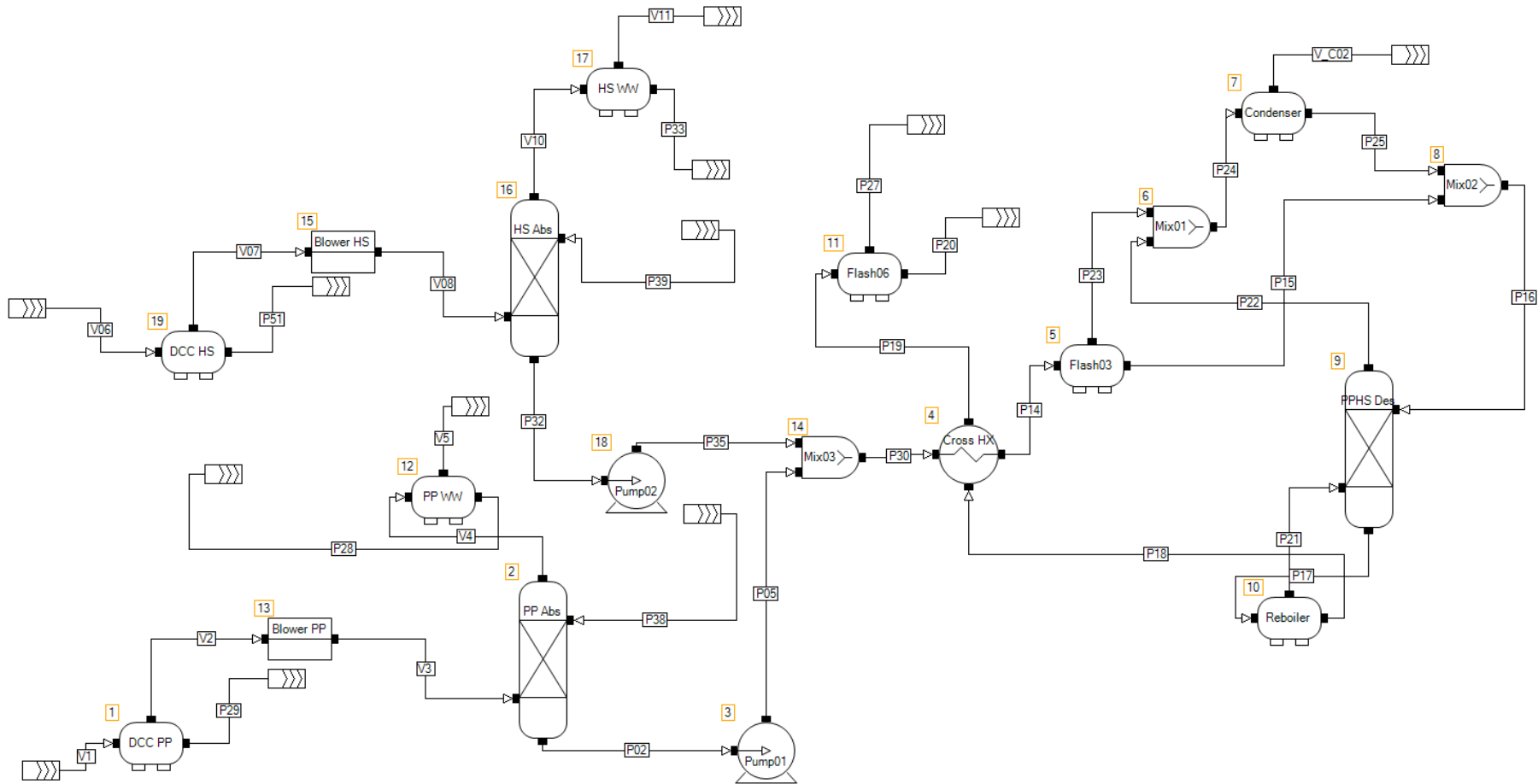
Buttons: More, Calculate

CO₂ SIM – simulation tool for post combustion capture

- Developed at SINTEF/NTNU
- CO₂ SIM gives specific methodology related to process optimization and handling of information flow
- Rigorous modeling approach
- Rate based mass and heat transfer models
- e-NRTL thermodynamics for CO₂-amine systems
- Tool for process optimization and design

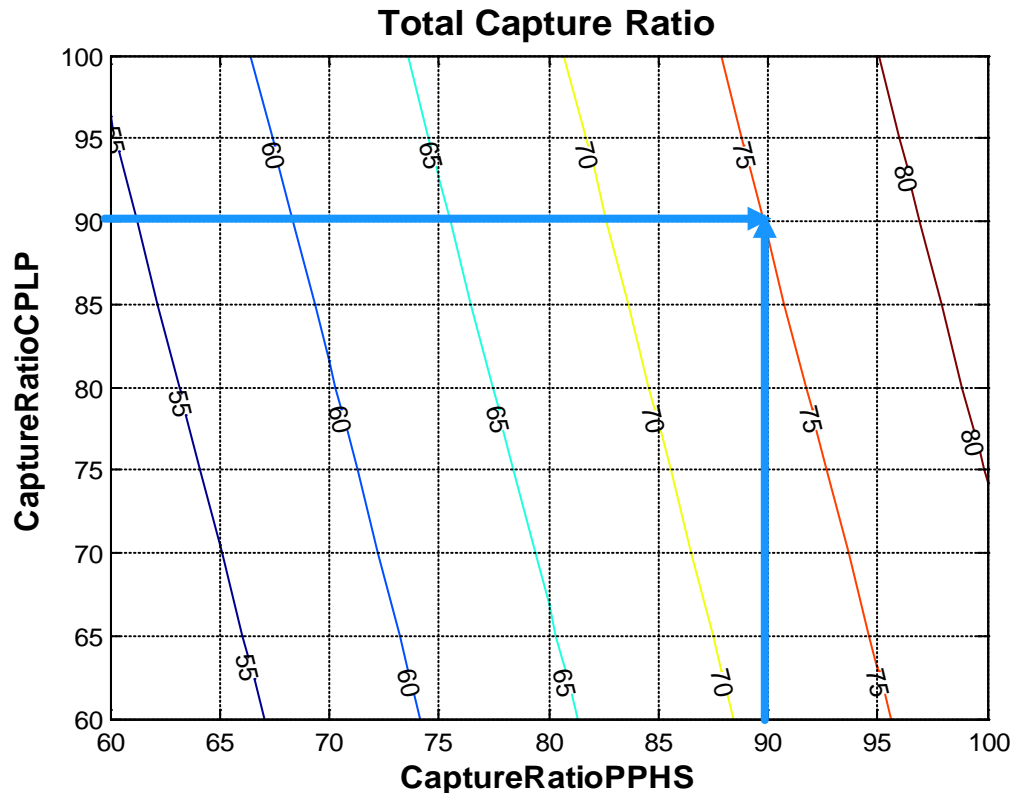


CO₂SIM case – Generic absorption process – single absorbers/common desorbers



Steam Generation, Hot stove + Coke, Lime Production flue gases together

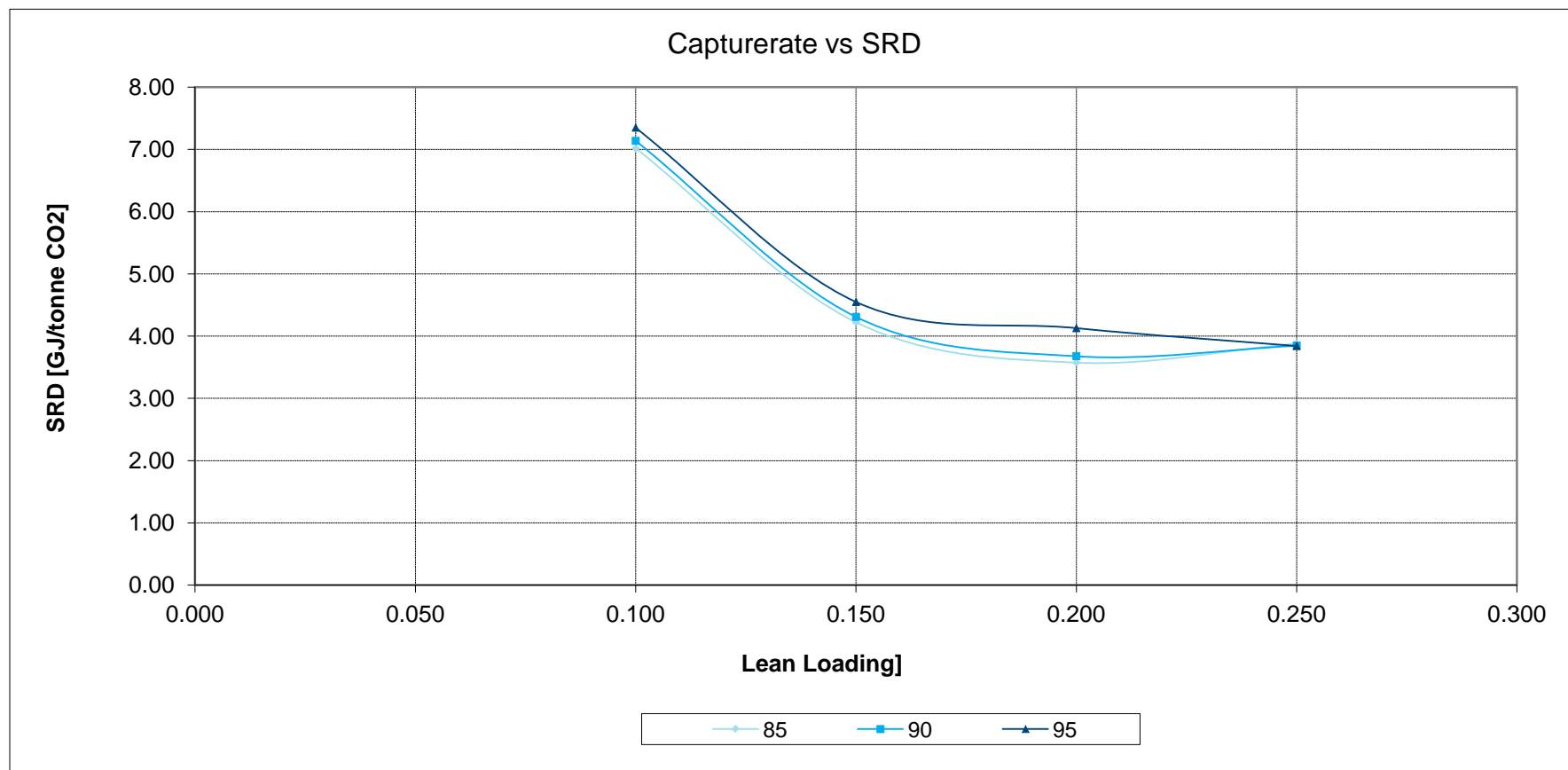
Total CO₂ recovery from the steel plant should be 75%



- 75% total CO₂ capture (of all 6 streams) is given by the red line. This shows that e.g. by capturing 96% in the *Steam Generation, Hot stove (PPHS)* case, 60% capture from the *Coke, Lime Production (CPLP)* case would be sufficient.

A 90% capture degree from both streams seem feasible, and fulfils the 75% target., disregarding the streams from the Sinter Plant and Reheating furnace

CO₂SIM optimization of solvent flow for case PP+HS, reference MEA



CO₂SIM results, 30wt %MEA reference

	CPLP 90%	PPHS 90%
Absorber A		
Packing height [m]	15	15
Column diameter [m]	6.3	11.3
Solvent Lean flow rate (tonne/h)	1,324	6,485
CO ₂ at inlet (mol %wet)	14.8 %	27.4 %
H ₂ O at inlet (mol %wet)	10.5 %	5.8 %
CO ₂ recovery (%)	90.0 %	90.0 %
CO ₂ Captured (tonne/h)	79	398
Absorber B		
Packing height [m]	15	15
Column diameter [m]	3.5	7.4
Solvent Lean flow rate (tonne/h)	505	2,784
CO ₂ at inlet (mol %wet)	19.8 %	27.3 %
H ₂ O at inlet (mol %wet)	12.7 %	6.3 %
CO ₂ recovery (%)	90.0 %	90.0 %
CO ₂ Captured (tonne/h)	31	171
Stripper		
Packing height [m]	9	9
Column diameter [m]	5.2	11.7
CO ₂ stripped [kg/hr]	110	568
Reboiler Duty [MW]	114	581
Specific Reboiler duty [GJ/tonn CO ₂]	3.73	3.68

Sizing of absorbers

Absorber column		PP	HS	CP	LP
Packing material		M2X	M2X	M2X	M2X
Specific surface	m ² /m ³	205.00	205.00	205.00	205.00
Diameter	m	11.3	7.4	3.0	2.8
Packing height	m	15	15	15	15
Packing surface pr. column	m ²	308 384	132 251	22 411	18 324
Number of beds, absorber packing		3	3	3	3
Height pr. bed.	m	5.0	5.0	5.0	5.0
Packing height WW-beds	m	2.0	2.0	2.0	2.0
Number of wash sections	m	2	2	2	2
Height required between sections	m	2.5	2.5	2.5	2.5
Height packed sections	m	29.0	29.0	29.0	29.0
Height mist collector + outlet section	m	2.5	2.5	2.5	2.5
Flue gas duct diameter	m	3.55	2.33	2.16	1.16
Absorber sump	m	3.0	3.0	3.0	3.0
Total absorber height	m	38.0	36.8	36.7	35.7



Packed column,
example (distillation)

Sizing of desorber

Desorber column		PP+HS	CP+LP
Packing height	m	9.00	9.00
Diameter	m	11.7	5.2
Cross section area single. des	m ²	107.5	21.2
Number of beds desorber packing		2	2
Height per bed	m	4.50	4.50
Height water wash section	m	2	2
Number of wash sections		1	1
Height between sections		2.5	2.5
Height packed sections	m	16.0	16.0
Height mist collector + gas ou	m	2.5	2.5
Height required for steam inlet	m	4	2
Desorber sump	m	2	2
Total desorber height	m	24.5	22.5



Packed column,
example (distillation)

Summary conventional plant with MEA

- For *conventional MEA based removal* of 75% of total produced CO₂ from the Steel plant:

CO ₂ Captured (tonne/h)	31	171
Specific Reboiler duty [GJt/ton CO ₂]	3.73	3.68

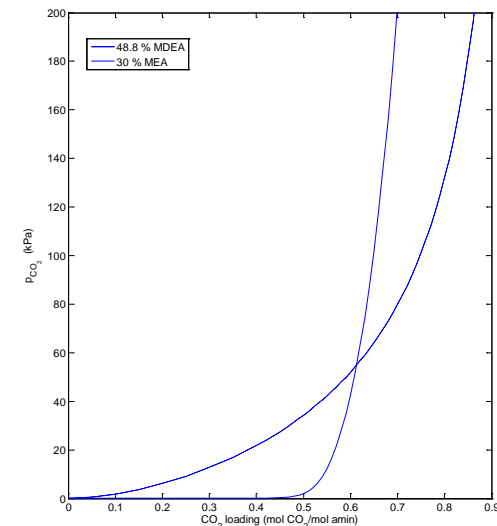
- Large process units (~8 megatonnes CO₂ per year is treated).
- **Necessary to look for ways to improve the capture process->**

Results new configuration + low energy solvent

- 1. Change to heat integration configuration – from 3.7 to 3.1 GJt/t with MEA (90% removal)
- 2. Heat integration scheme and new solvent – below 2.7 GJt/t

CO₂ capture from Oxygen Blast Furnace – OBF case

- OBF gas has a pressure of 4.1 bar and 34% CO₂, $p_{\text{CO}_2} = 1.4$ bar
 - CO₂ partial pressure is 10 times larger than e.g. the Coke Plant flue gas
- This enables a significant reduction of the capture energy requirement
- Thermodynamic potential for energy saving due to less work for the compression of CO₂ from the mixture conditions to the pure CO₂ product
- Lower volume flow of gas, -reduced size of absorber unit
- Absence of O₂ in the gas
 - significantly reduced solvent degradation to be expected
- MDEA or AMP based solvents are able to utilize the pressure benefit and are better suited than MEA for the current case
 - Chosen base case: 40% MDEA with 10% piperazine as activator, process offered commercially by several vendors



Summary and conclusions OBF case

- Simulations showed that the resulting energy requirement was 2.35 GJt/ton CO₂ or 257 MMt in total
 - Using an intercooled absorber with MDEA/Pz solvent.
- Capture of 3.2 Mt CO₂/year from OBF gas/94%CO₂ capture
- Absorber:
 - Diameter: 9m
 - Packing Height 14m
- Desorber:
 - Diameter: 8.52m
 - Packing height: 6m

Summary and conclusions (1)

- *Conventional 'end gases'*
- Utilization of new solvent systems and improved and optimized process configuration will significantly increase the efficiency of the CO₂ capture process.
- Improving the process configuration with MEA shows that the energy requirement can be reduced down to ~3.1 GJ/ton
- In addition changing to a new solvent (activated sterically hindered amine) makes it possible to reduce energy requirement down to 2.7 GJ/ton.

Summary and conclusions (2)

- *CBF gases*
- "Non-Solvent-optimized" example gave SRD of 2.35 GJ/ton
- Chemical absorption is well suited for CO₂ removal from CBF top gases.
- Note: Not use of high reacting amines (MEA) but formulated solvents for the particular solvent partial pressure (High CO₂ solvent carrier with activator) Could be an amino acid system
 - High CO₂ content, large removal rate (94% capture) as well as no oxygen content.