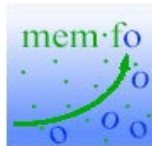
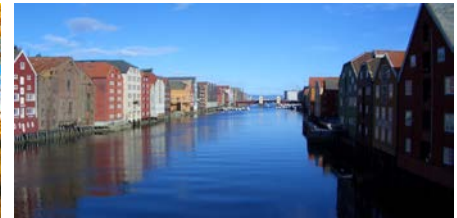


# CFD Modeling of Hollow Fiber Membrane Contactor for Post-Combustion CO<sub>2</sub> Capture



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# Outline

## ☐ Introduction

- Mass Transfer in a gas/liquid membrane contactor

## ☐ Development of CFD model

## ☐ Results and discussion

- Characterization of Liquid/gas film resistance
- Influence of membrane to overall mass transfer
- Influence of chemical reaction to overall mass transfer

## ☐ Conclusions

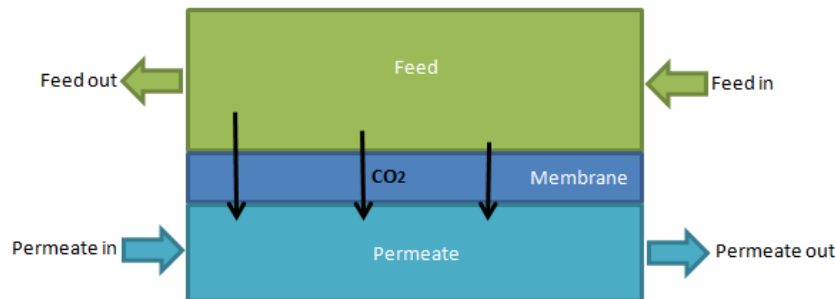
# Introduction

## Membrane contactor; a hybrid technology

### ❑ Compared to absorption columns

- Larger sp. surface area, linear scale-up, modular design, flexible operation

Contractors	Sp surface area (m <sup>2</sup> /m <sup>3</sup> )	Reference
Free dispersion column	1-10	Reed et al. (1995)
Mechanically agitated column	50-150	Westerterp et al. (1984)
Packed column	100-800	Reed et al. (1995)
Membrane contactor	1500-3000	Kumar et al. (2002)



Amine  
Absorption  
Unit

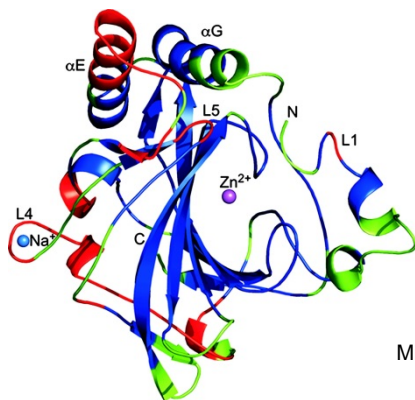
Air Liquide

Membrane Unit

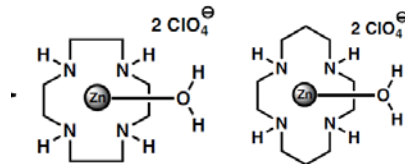
# Introduction

## □ Membrane contactor for flue gas treatment

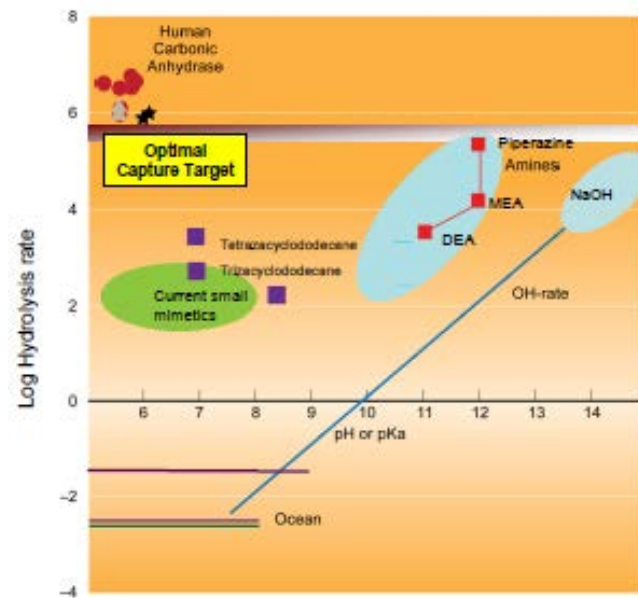
- High and non dispersive contact offers efficient mass transfer
- Highly reactive Carbonic anhydrase (CA) and mimic CA with reaction rate **4000 times faster than MEA** to account for low mass transfer driving force



Carbonic Anhydrase Molecular structure



Mimic Carbonic Anhydrase Molecular structure

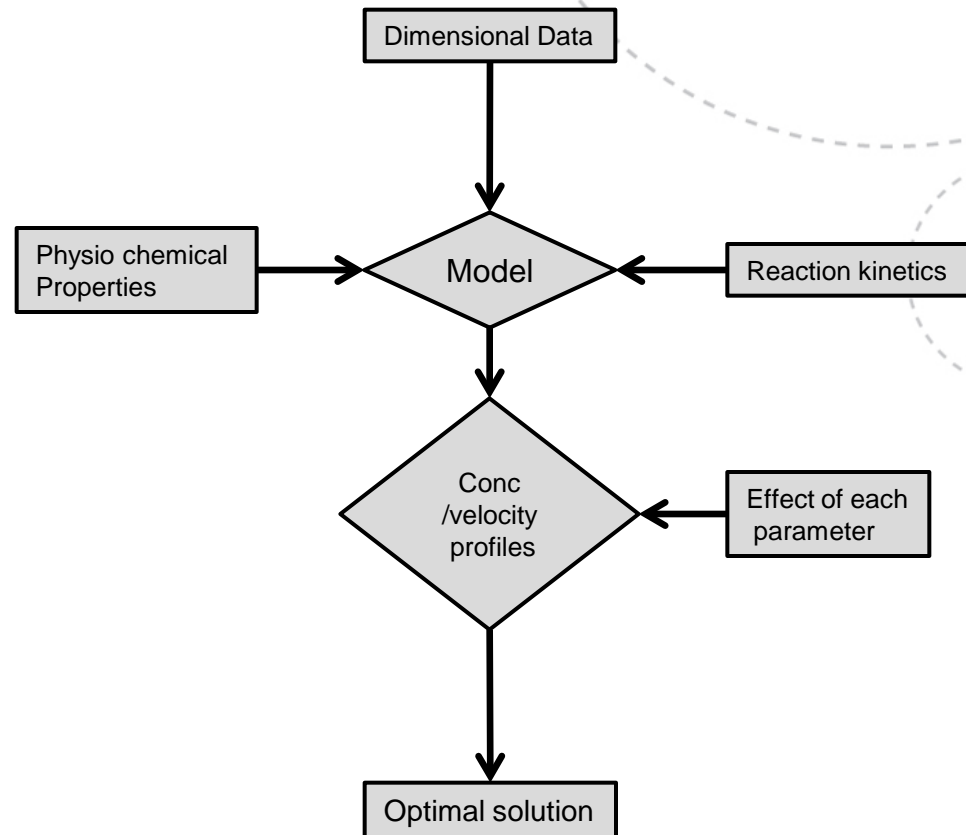


Hydration rate of CO<sub>2</sub> by various absorbents.  
Aines R. H Lawrence Livermore National Laboratory

# Scope

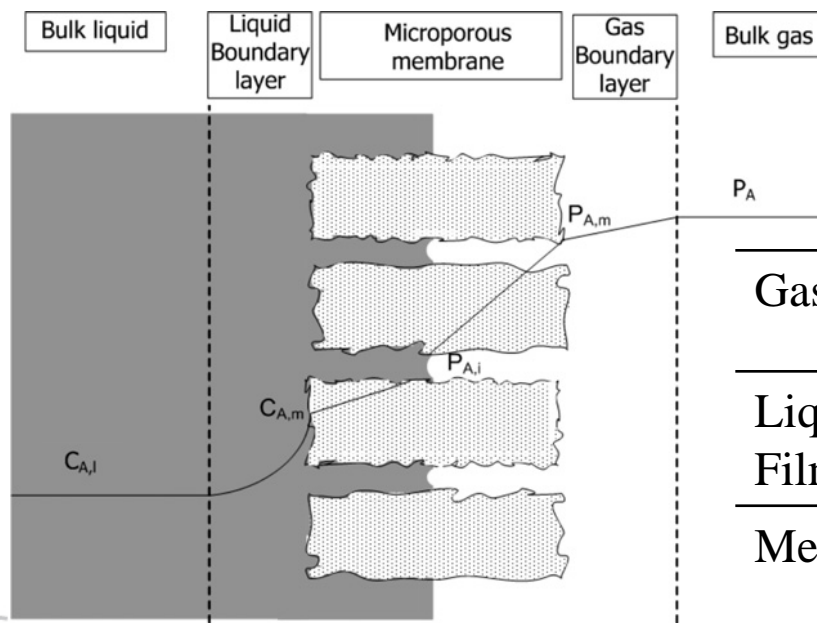
## ■ This work

- CFD model of a membrane contactor with physical and chemical absorption by using **Multi physics COMSOL**
- Carbonic anhydrase (CA) and mimic CA for reactive absorption of CO<sub>2</sub>
- Mass transfer through a micro porous, hydrophobic membrane
- Developed model to suggest an optimal set of parameters for designing operations of a membrane contactor.



# Mass Transfer in Membrane Contactor

- Overall mass transfer in a membrane contactor is analogous to heat transfer and can be exemplified by resistance in series model.



$$\frac{1}{K_{ov}} = \frac{1}{k_l} + \frac{1}{k_m} + \frac{1}{k_g}$$

Gas Film	$u \frac{\partial C_A}{\partial z} = D_{Ag} \left[ \frac{1}{r} \frac{\partial}{\partial r} \left( r \cdot \frac{\partial C_A}{\partial r} \right) \right]$
Liquid Film	$v \frac{\partial C_A}{\partial z} = D_{AL} \left[ \frac{1}{r} \frac{\partial}{\partial r} \left( r \cdot \frac{\partial C_A}{\partial r} \right) \right] - R_A$
Membrane	$D_{Am} \left[ \frac{\partial^2 C_A}{\partial r^2} + \frac{1}{r} \left( \frac{\partial C_A}{\partial r} \right) + \frac{\partial^2 C_A}{\partial z^2} \right] = 0$

CO<sub>2</sub> concentration profile in a membrane contactor adapted from **Journal of Membrane Science 380 (2011) 21– 33**

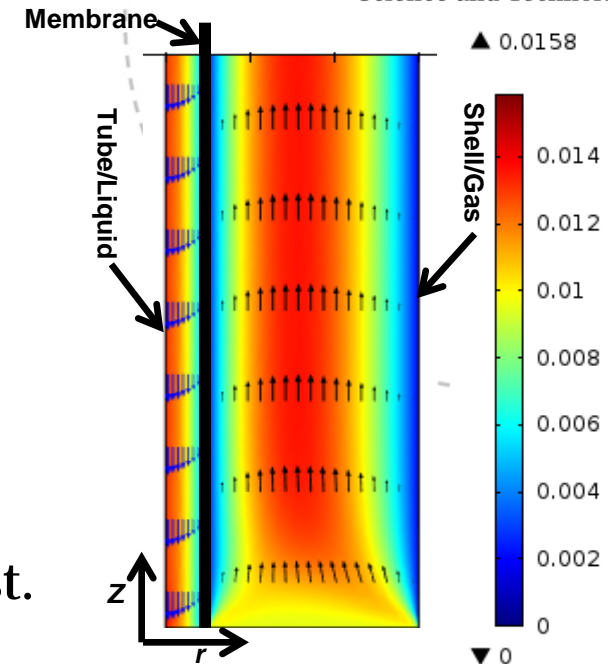
# Model development

## Assumptions

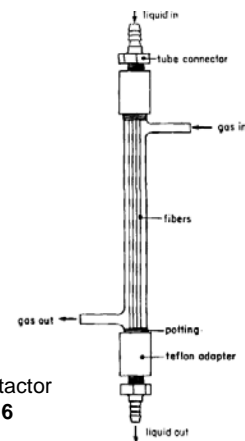
- Regular and uniform pores
- Hydrophobic membrane
- First order reaction between CO<sub>2</sub> and catalyst.

## Model Basis

- Velocities are adjusted to maintain a laminar regime
- Flue gas containing 10% CO<sub>2</sub> at 1 bar and 25°C.
- Carbonic Anhydrase (CA) and mimic CA catalyst to promote the absorption in liquid



Velocity profile in gas/ liquid phase



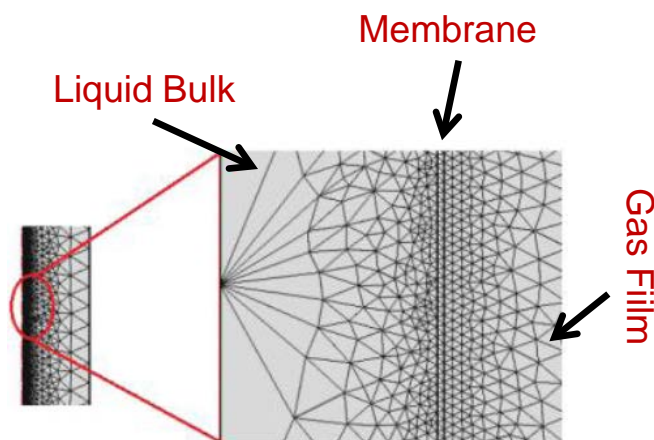
Longitudinal hollow fiber membrane contactor  
 AIChE Journal 1986,32,11 1910-16



# Model development (cont...)

Basis for model geometry

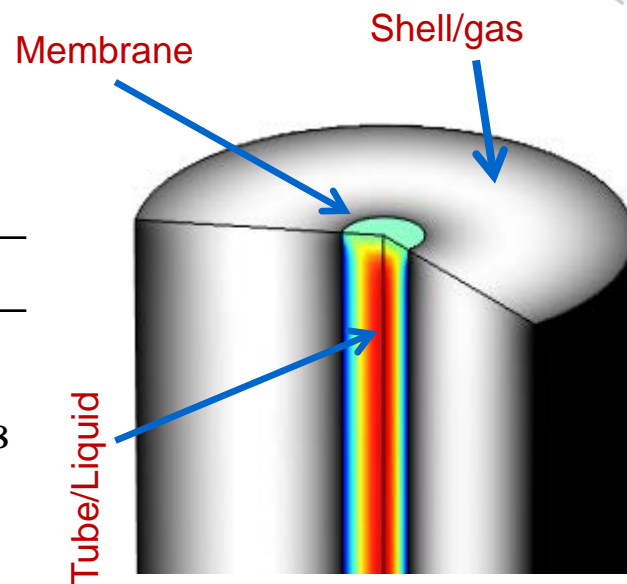
- In this work **Finite Element Method** is used for calculations.



Finite element with physics controlled size

Parameter	Symbol	Value
Length	L	100mm
Radius of membrane	$R_1$	1 mm
Radius of shell	$R_2$	6mm
Porosity	$P_{or}$	0.7
Tortuosity	$T_{or}$	2
Conc. in gas phase	$C_o$	10 %

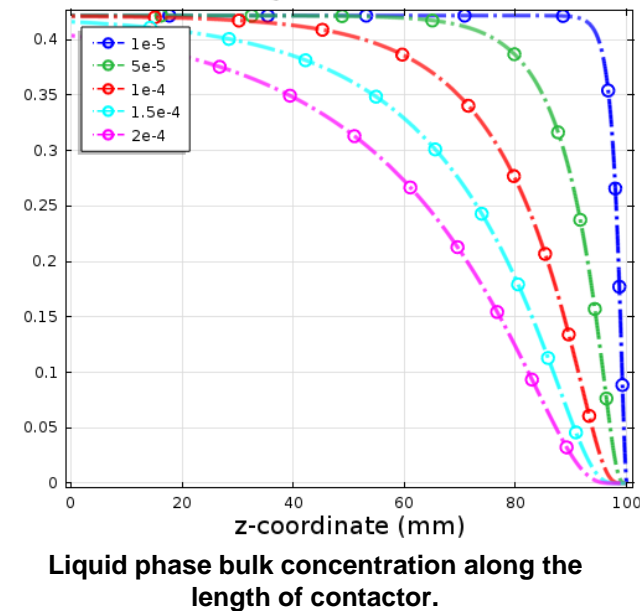
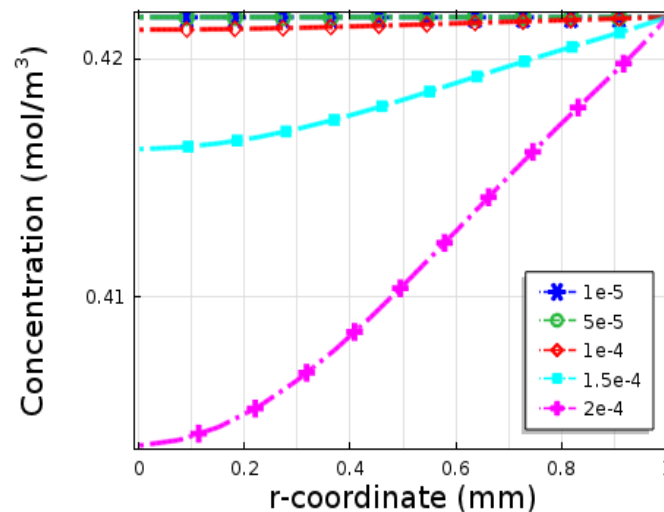
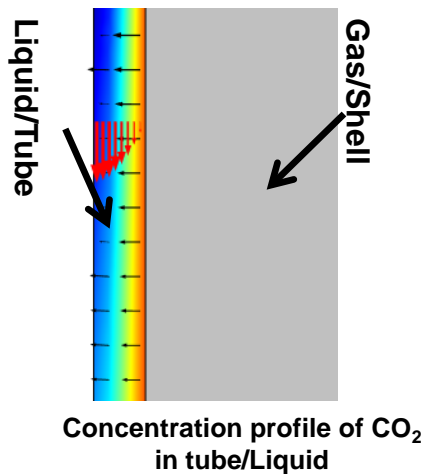
Literature	Value	Source
Diffusivity in Shell	$1.5 \times 10^{-5} \text{m}^2/\text{S}$	Reid, R. C.; Prausnitz, 1986
Diffusivity in water	$1.92 \times 10^{-9} \text{m}^2/\text{S}$	Chem. Eng. Comm., 1996, 144,113-158
Partition coefficient	$1.205 \times 10^{-2}$	J. Chern. Eng. Data, 1988, 33, 29-34,
Reaction rate of MEA	5920 (1/s)	Chem Eng. Sci. 2007,39,207-25





# Results and Discussion

## Physical absorption of CO<sub>2</sub> in liquid

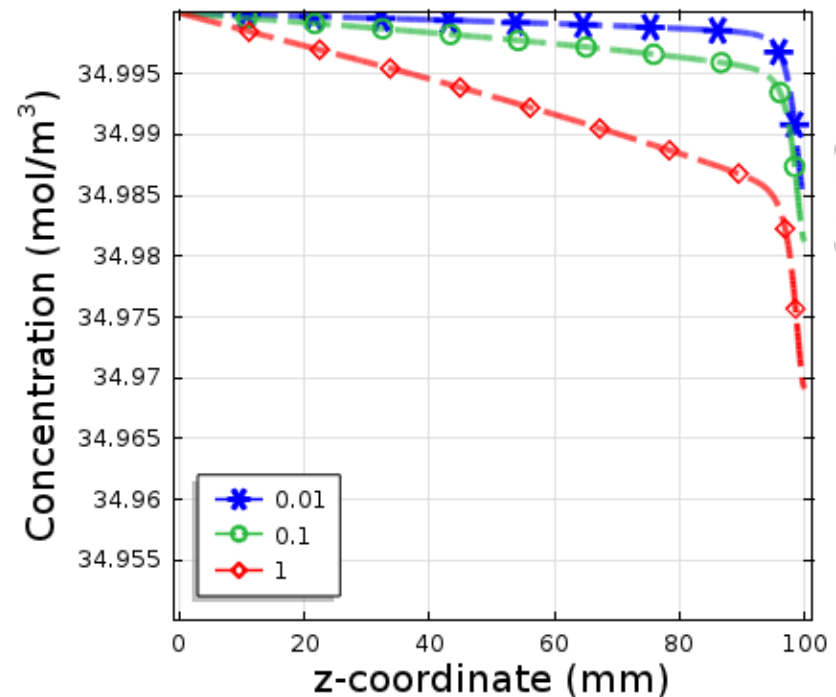
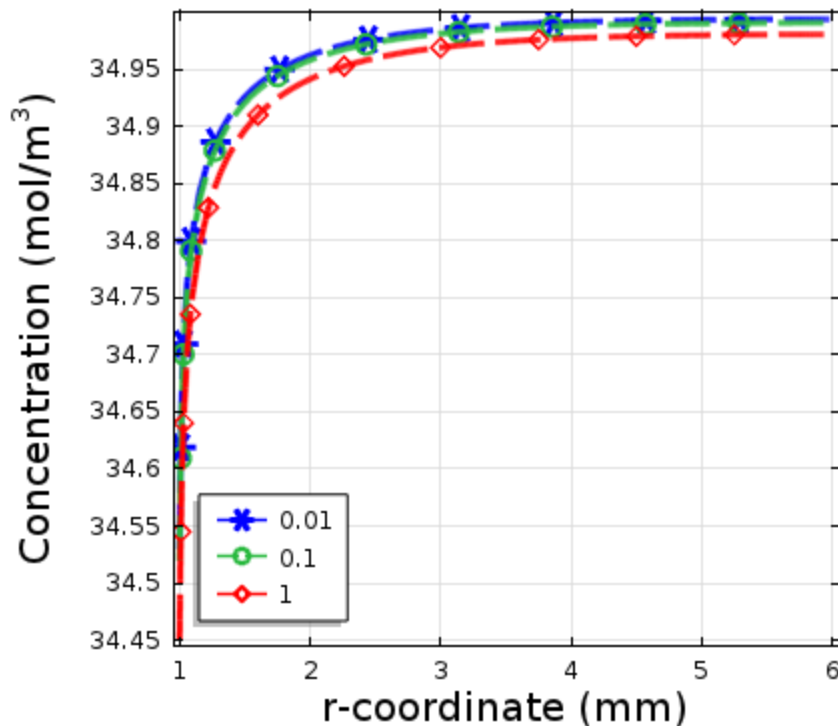


Liquid velocity changing from 1e-5 to 1 m/s

Appreciable effect on liquid loading.

# Results and Discussion

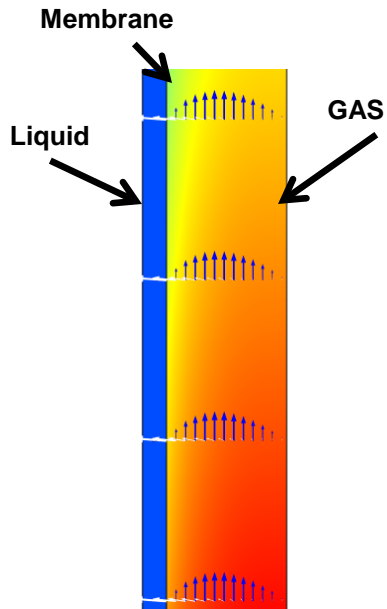
## Physical absorption of CO<sub>2</sub> in liquid



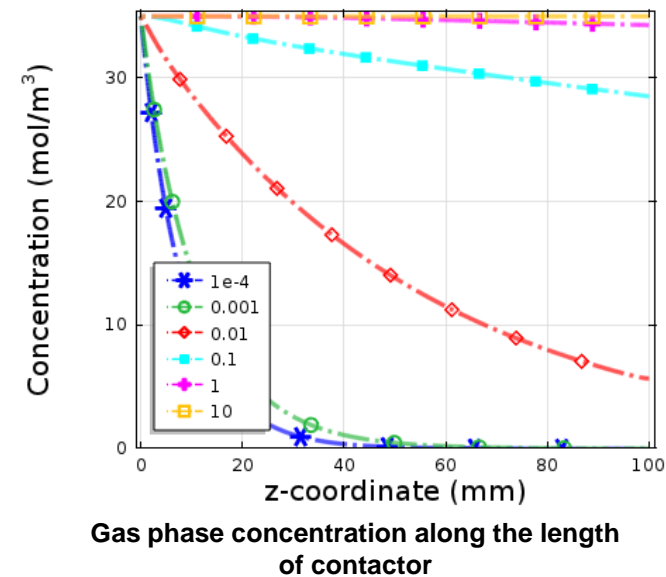
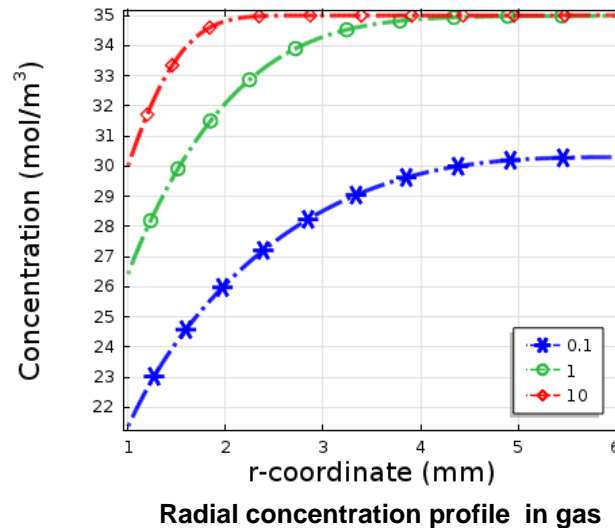
- **Appreciable effect on liquid loading.**  
**However, no significant effect on gas phase**

# Results and Discussion

## □ Characterization of Gas film resistance



Concentration profile of  $\text{CO}_2$   
in shell and tube



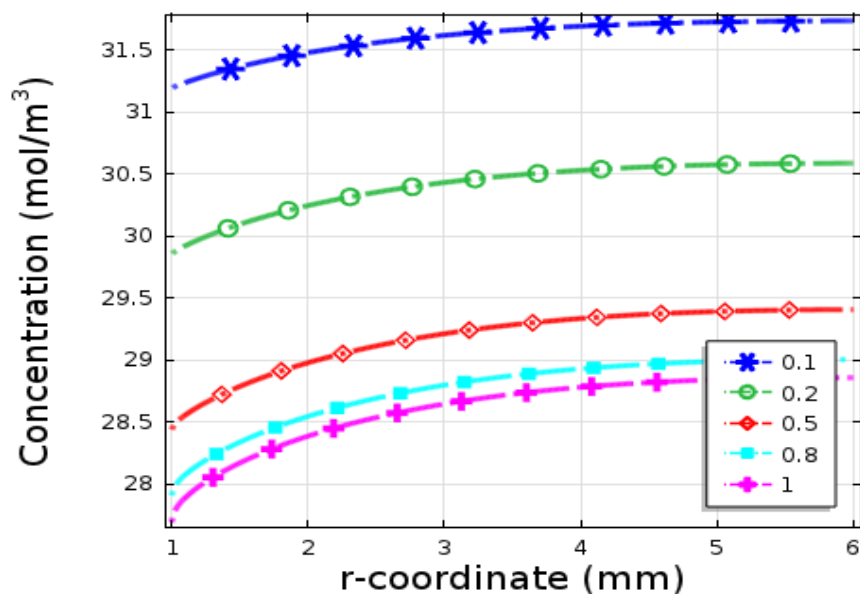
Investigated gas velocity:  $1\text{e-}4$  to  $10\text{ m/s}$

Appreciable effect of gas velocity at interfacial concentration shows that mass transfer limitation has now moved from liquid film to gas film/membrane.

# Results and Discussion

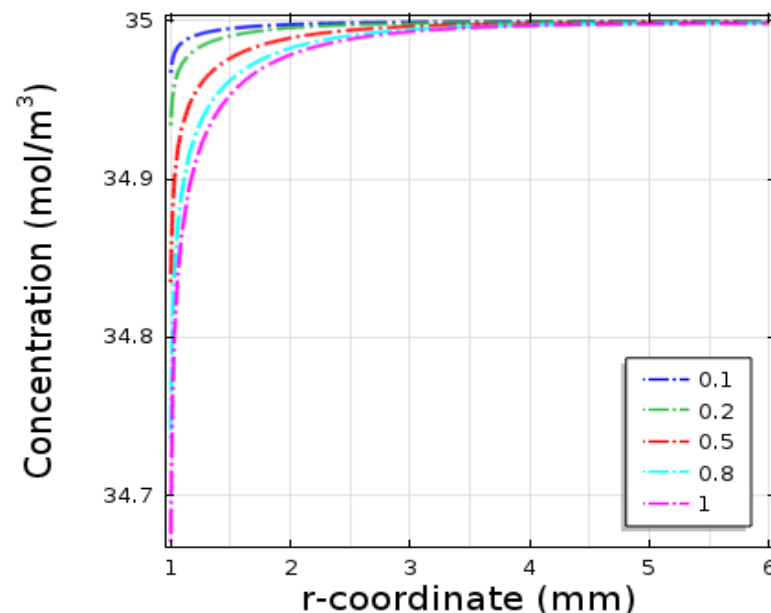
## □ Influence of porosity

### Chemisorption



Gas phase radial concentration. porosity

### Physical absorption



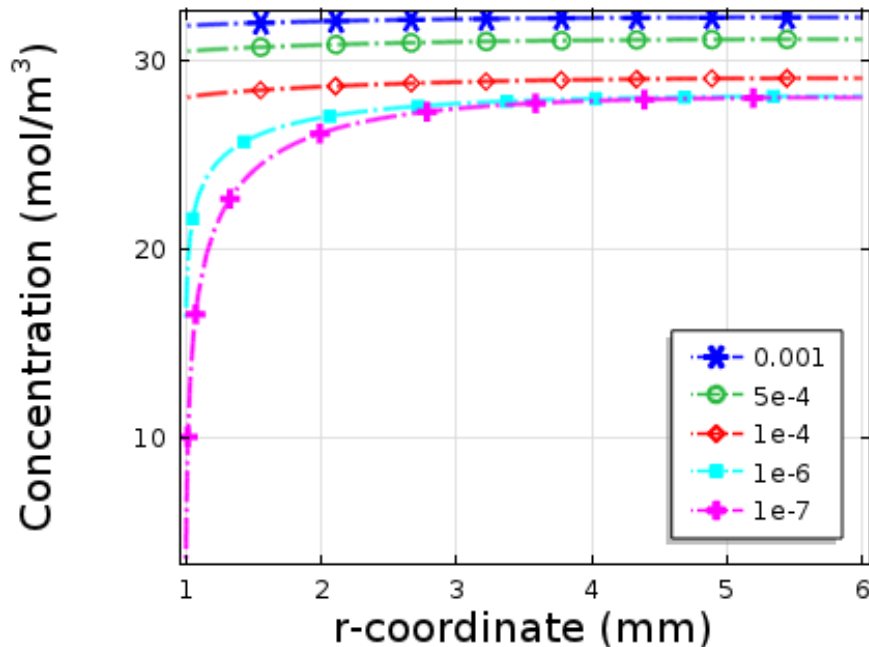
Gas phase radial concentration. porosity

Porosity of membrane varied from 0.1 to 1.

Membrane resistance has significant contribution to mass transfer in chemical absorption.

# Results and Discussion

## □ Influence of membrane thickness

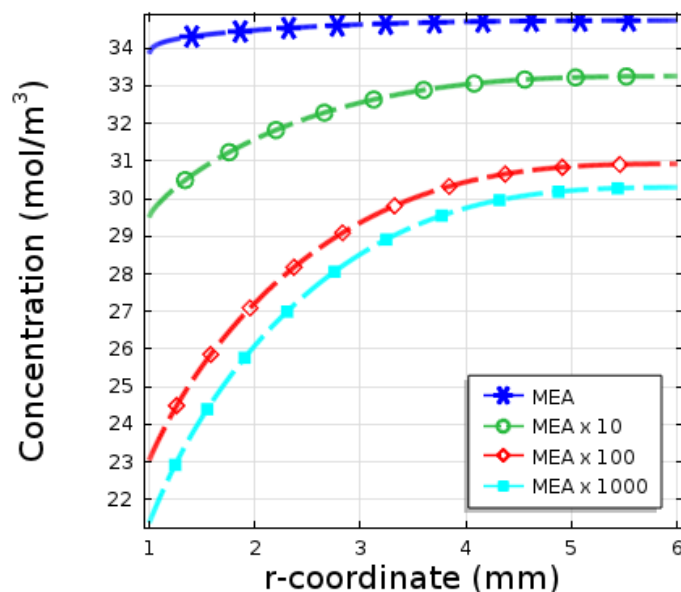


Gas phase radial concentration at varies membrane thickness

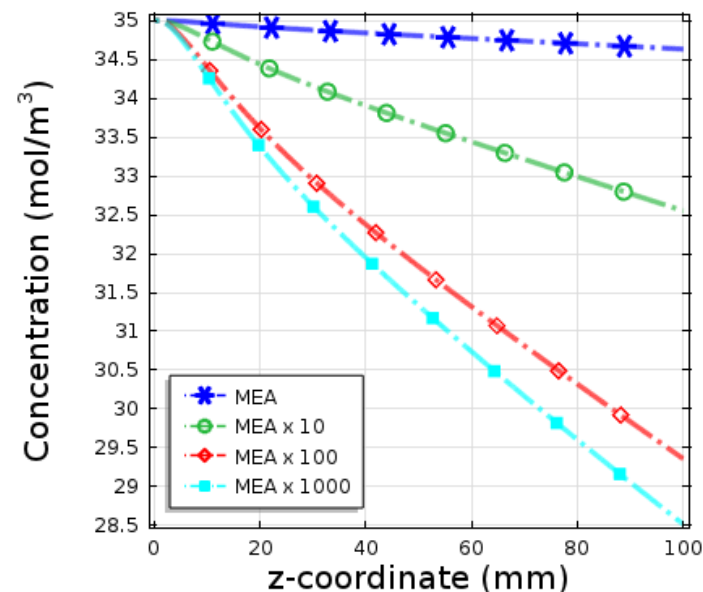
- Thickness of membrane was varied between 1 mm and 1e-4 mm.
- Thickness of membrane does have a significant effect on mass transfer but **developing a self supported membrane of 1e-4 mm is challenging.**

# Results and Discussion

## □ Influence of Reaction



Gas phase radial concentration at various reaction rates



Gas phase axial concentration at various reaction rates

Reaction rate varied 10, 100 and 1000 times that of MEA.

With increase in reaction rate, a significant increase in efficiency is observed

# Conclusions

- For Physical absorption, liquid film resistance is the limiting factor to mass transfer.
- For Chemisorption mass transfer resistance shifts to membrane and gas film.
- Membrane porosity and thickness contributes significantly to mass transfer in chemical absorption.
- This work is a guideline to design a membrane contactor operating with and without chemical reaction.



Pump

Tube  
Bundle

vessel

Membrane

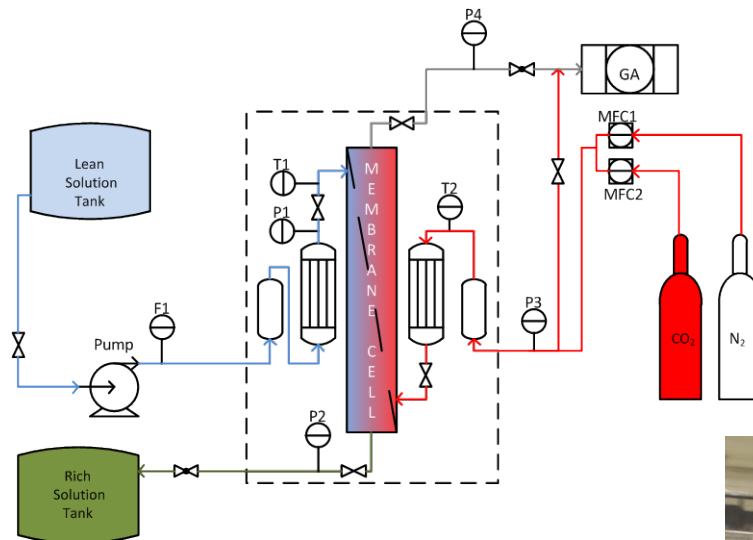
Analyser

Indicator

Cylinder

Gate valve

Globe valve



# Thank you for your attention!



*Special thanks to:*

- *Dr Ardi Hartono*
- *Mr Hassan Ali*