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Sensitivity analysis of post-combustion CO₂ capture at pilot scale level

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Synopsis

- Objectives
- PACT facility
- Solvent based carbon capture plant
- SCCP model in Aspen HYSYS
- Model validation for 4.5 mol% CO₂
- Sensitivity analysis study
- Sensitivity variation cases
- Conclusions



Objectives

- To understand the process operation of the post-combustion capture system in a closed-loop.
- Estimation of the operability range of the post-combustion capture plant (MEA system) at pilot-scale through process sensitivity analysis.
- Operational parameters** are varied, such as:
 - L/G ratio
 - Flue gas temperature
 - CO₂ composition in flue gas**
 - Liquid temperature
 - Lean loading
 - CO₂ capture rate**
 - Amine strength
 - Stripper pressure
- Performance parameters** include:
 - Specific reboiler duty**
 - Rich loading
 - Absorber temperature profile**
 - Stripper temperature profile



UK CCS Pilot-Scale Advanced Capture Technology (PACT*) Facility

- ❑ Deals with a variety of solvents.
- ❑ Capacity : **1 ton/day of CO₂ (based on MEA)**.
- ❑ Units: absorber, stripper, water wash column, cross heat exchanger, reboiler and condenser.
- ❑ Flue gas desulphurization through carbonate wash.
- ❑ Dedicated control system.
- ❑ Integration with:
 - ❑ 250 kW air/oxy fired combustion plant.
 - ❑ 300 kW gas turbine.

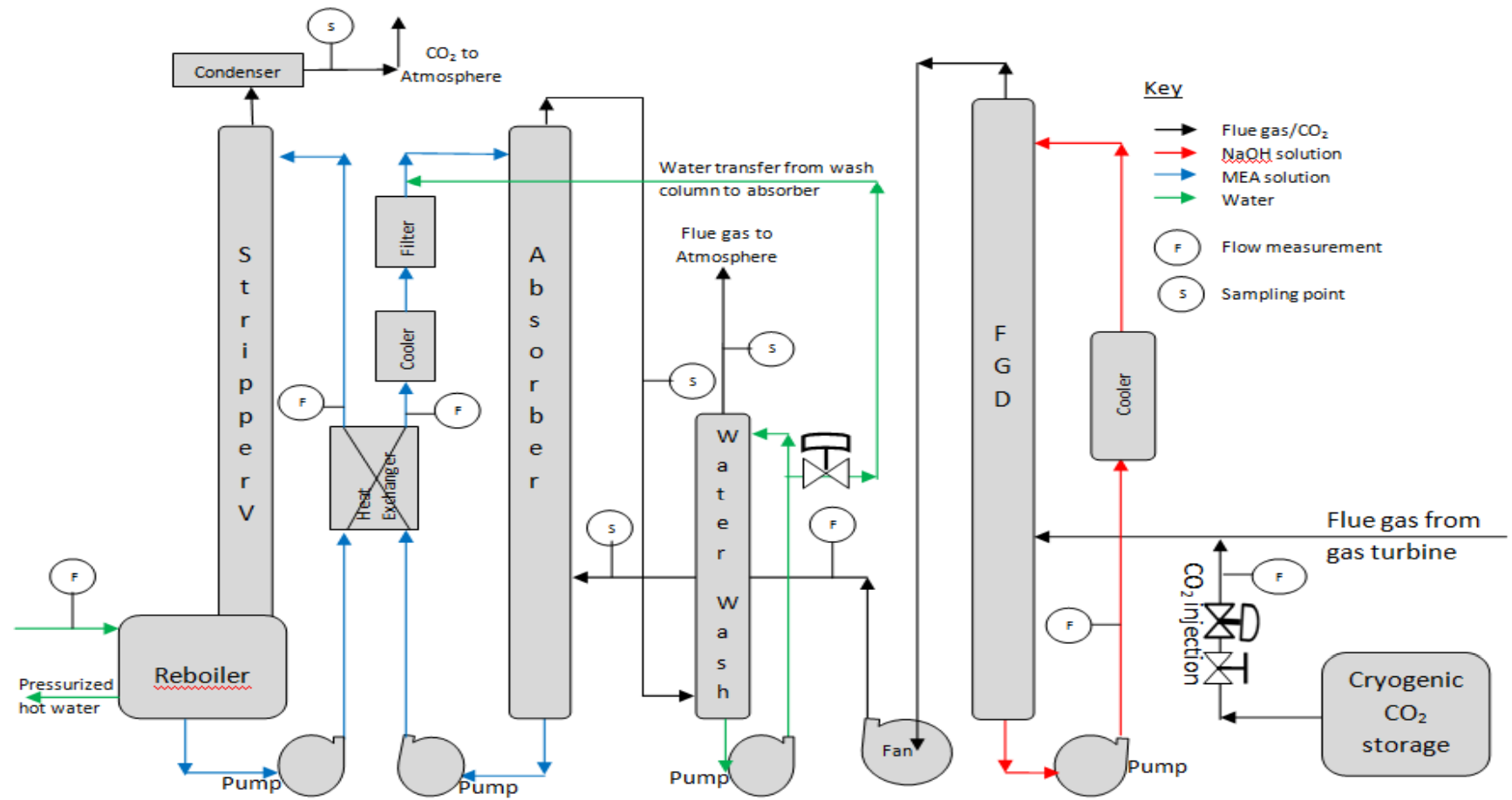


SCCP Plant

* www.pact.ac.uk



Solvent based Carbon Capture Plant

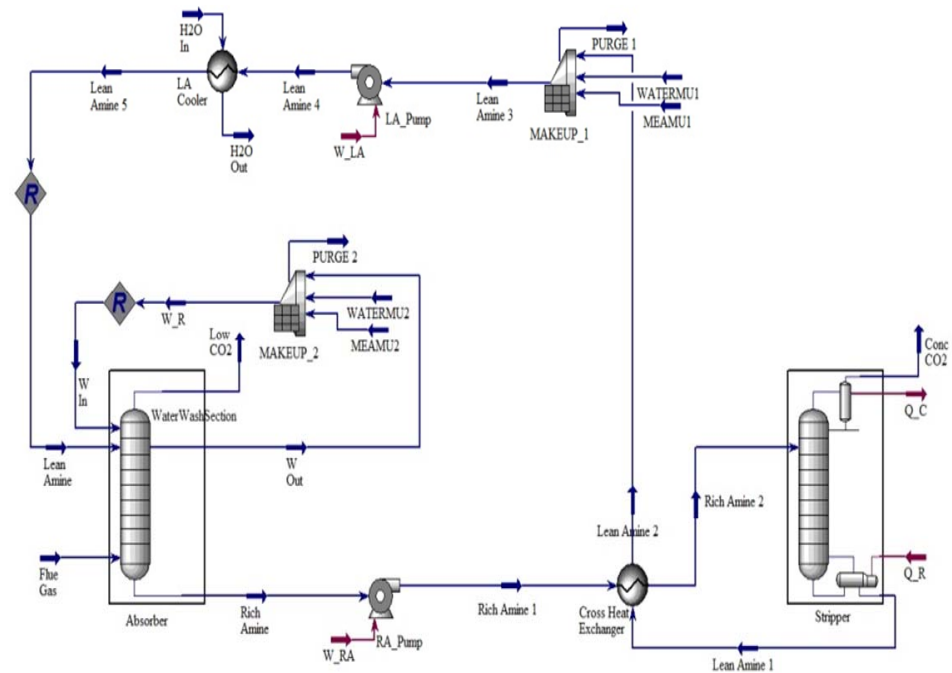


Schematic of Solvent based Carbon Capture Plant (SCCP).



SCCP Model In Aspen HYSYS

- ❑ Property Package: **Acid Gas** (Rate base method).
- ❑ Mass Transfer method: Bravo-Fair
- ❑ Interfacial Area method: Bravo-Fair
- ❑ Packing Pressure Drop Correlation: Vendor Specified
- ❑ Packing Type: **IMTP(25mm)**
- ❑ **Absorber:**
Height = 3 + 3 m
Diameter = 0.303 m
- ❑ **Water Wash Section:**
Height = 1.2 m
Diameter = 0.303 m
- ❑ **Stripper:**
Height = 3 + 3 m
Diameter = 0.303 m



Post-combustion capture plant model developed in Aspen HYSYS® V8.6.



Model Validation at 4.5 mol% CO₂ in flue gas

Parameter	Experimental Value	Simulated Value
Lean amine flow rate, (kg/hr)	515.6	515.6
Lean CO ₂ loading, (mol/mol)	0.25	0.25
Rich amine flow rate, (kg/hr)	531	531.4
Rich CO ₂ loading, (mol/mol)	0.41	0.411
CO ₂ in flue gas, (kg/hr)	18.2	18.2
CO ₂ captured, (kg/hr)	16.5	16.51
Reboiler duty, (kW)	27	25.3
Specific Reboiler duty, (MJ/kgCO ₂)	5.92	5.51



Sensitivity Analysis Study

Set No.	Sensitivity Analysis	Type
Set A	Variation of CO₂ composition in flue gas (5.5 mol% $\geq y_{\text{CO}_2} \leq$ 9.9 mol%)	Experimental and Modelling
Set B	Variation of CO₂ capture rate (60% $\geq \psi \leq$ 95%)	Experimental* and Modelling
Set C	Variation of liquid flow rate (0.6 $\geq L/G \leq$ 2.6)	Modelling
Set D	Variation of amine strength (20wt% $\geq \omega \leq$ 36wt%)	Modelling
Set E	Variation of lean amine loading (0.10 $\geq \alpha \leq$ 0.35)	Modelling
Set F	Variation of flue gas temperature (30°C $\geq T_G \leq$ 50°C)	Modelling
Set G	Variation of liquid temperature (30°C $\geq T_L \leq$ 50°C)	Modelling
Set H	Variation of stripper pressure (1.2bar $\geq P_s \leq$ 2.2bar)	Modelling

*experimentally CO₂ capture rate is varied from 90 to 94.4%

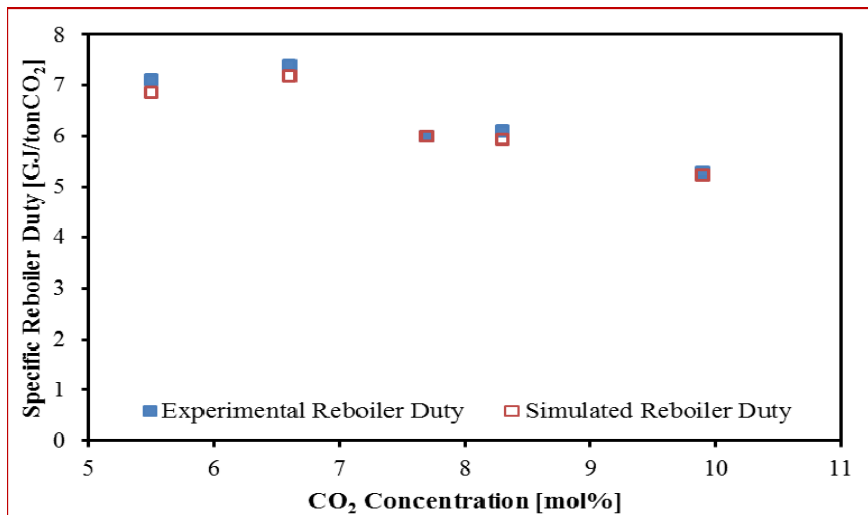


Set A: Variation of CO₂ composition in flue gas (1/2)

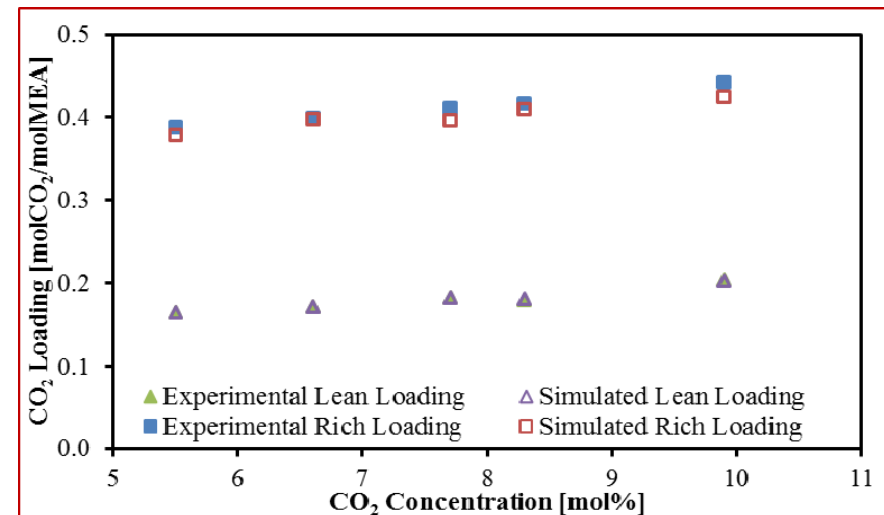
Validation

Variation:

- ❑ $5.5\text{mol}\% \geq y_{\text{CO}_2} \leq 9.9\text{mol}\%$
- ❑ $\omega = \sim 30\text{wt}\%$
- ❑ $\psi = \sim 90\%$
- ❑ $T_G = 40^\circ\text{C}$ and $T_L = 40^\circ\text{C}$
- ❑ $P_s = 1.2\text{bar}$



Measured and simulated lean and rich CO₂ loading versus CO₂ concentration.



Measured and simulated data specific reboiler duty versus CO₂ concentration.

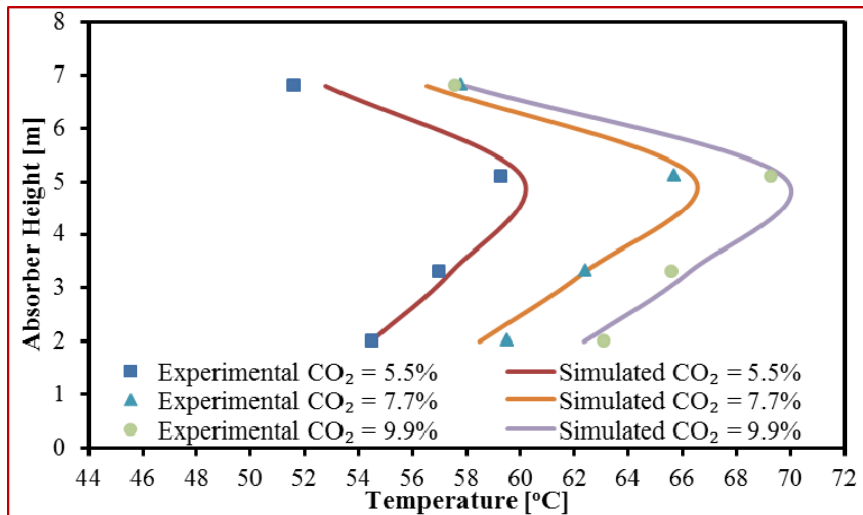


Set A: Variation of CO₂ composition in flue gas (2/2)

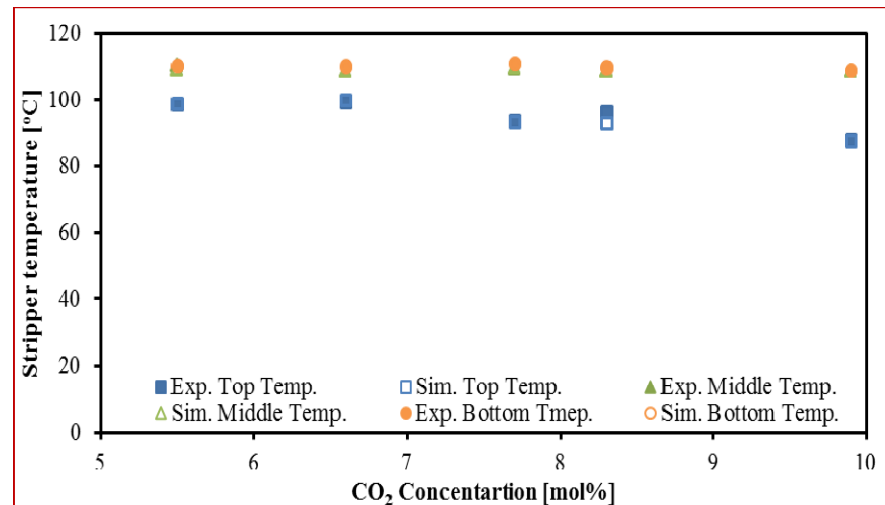
Validation

Variation:

- ❑ $5.5\text{mol}\% \geq y_{\text{CO}_2} \leq 9.9\text{mol}\%$
- ❑ $\omega = \sim 30\text{wt}\%$
- ❑ $\psi = \sim 90\%$
- ❑ $T_G = 40^\circ\text{C}$ and $T_L = 40^\circ\text{C}$
- ❑ $P_s = 1.2\text{bar}$



Measured and simulated absorber temperature profile for different CO₂ concentrations.



Measured and simulated stripper temperature profile for different CO₂ concentrations.

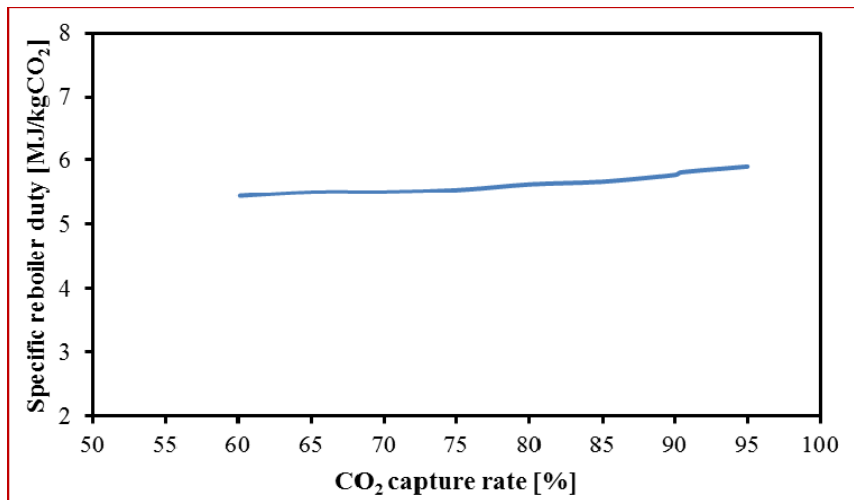


Set B: Variation of CO₂ capture rate

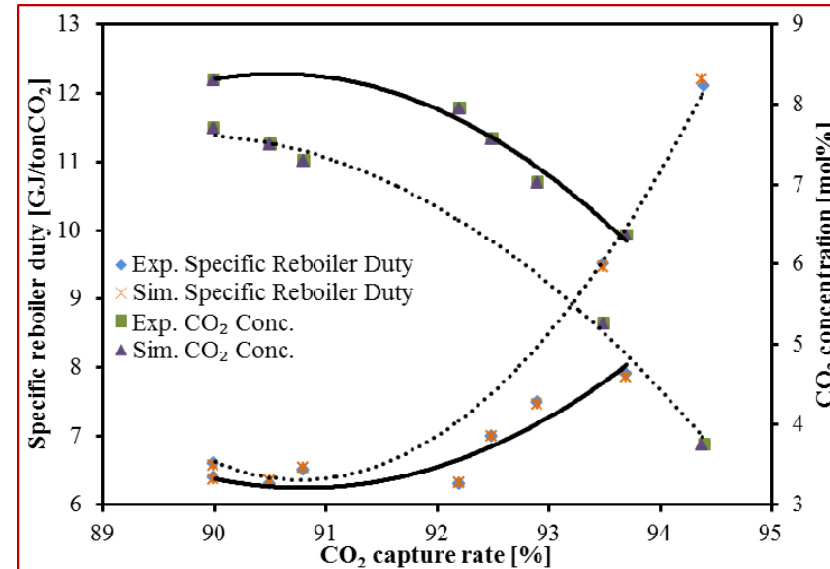
Validation

Variation*:

- $y_{CO_2} = 4.5\text{mol}\%$
- $L/G = 1.9$
- $\alpha = 0.25$ and $\omega = 28.5\text{wt}\%$
- $60\% \geq \psi \leq 95\%$
- $T_G = 40^\circ\text{C}$ and $T_L = 40^\circ\text{C}$
- $P_s = 1.2\text{bar}$



CO₂ capture rate versus specific reboiler duty.



Measured and simulated specific reboiler duty and CO₂ concentration versus CO₂ capture rate for different flow rates.

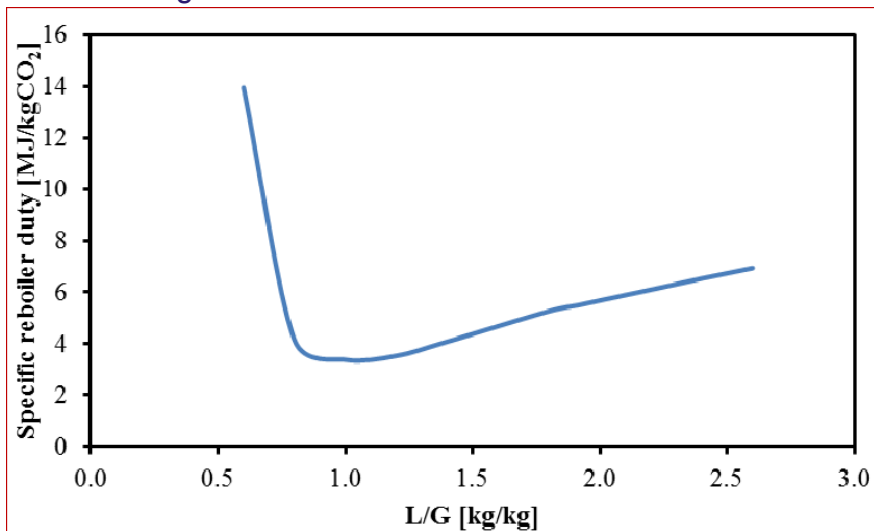
*for modelling results only.



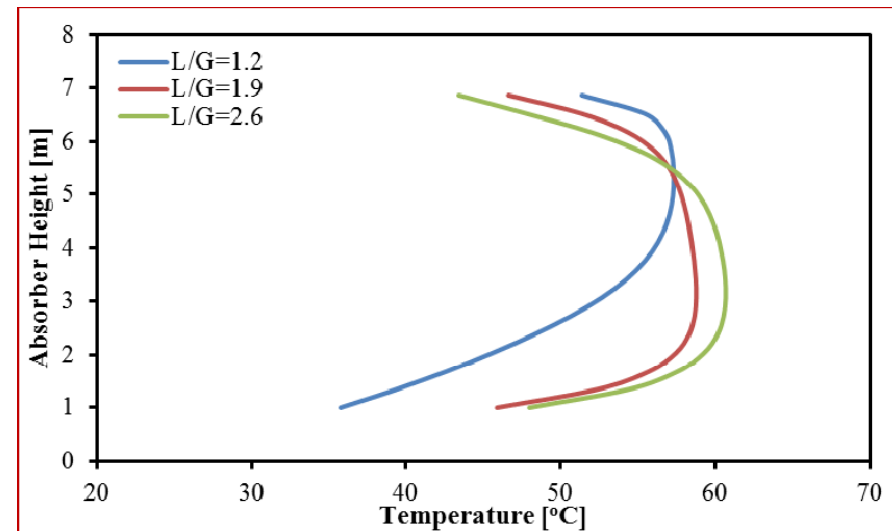
Set C: Variation of liquid flow rate

Variation:

- $y_{\text{CO}_2} = 4.5\text{mol}\%$
- $0.6 \geq L/G \geq 2.6$
- $\alpha = 0.25$ and $\omega = 28.5\text{wt}\%$
- $\psi = 90\%$
- $T_G = 40^\circ\text{C}$ and $T_L = 40^\circ\text{C}$
- $P_s = 1.2\text{bar}$



L/G ratio versus specific reboiler duty.



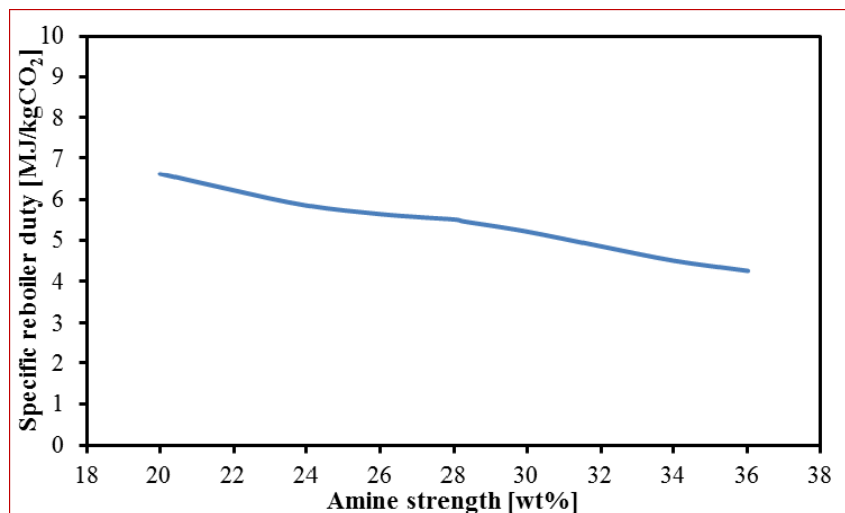
Absorber temperature profiles.



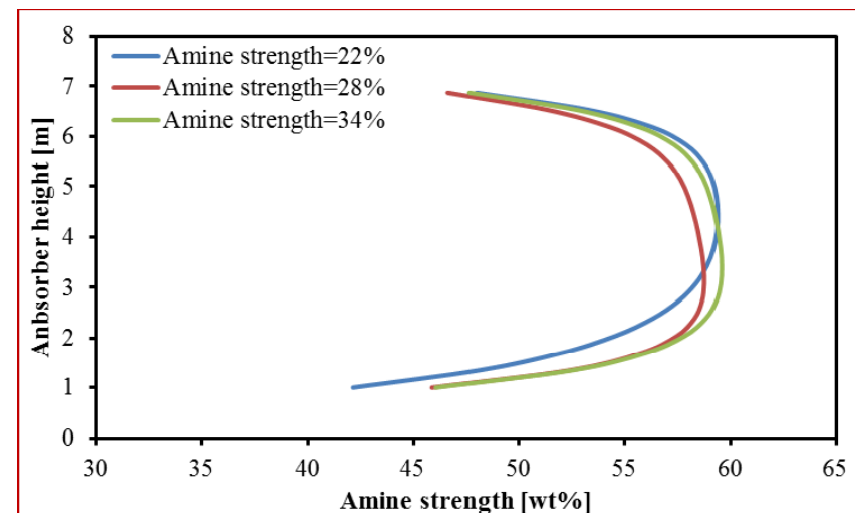
Set D: Variation of amine strength

Variation:

- $y_{\text{CO}_2} = 4.5\text{mol}\%$
- $L/G = 1.9$ and $\alpha = 0.25$
- $20\text{wt}\% \geq \omega \leq 36\text{wt}\%$
- $\psi = 90\%$
- $T_G = 40^\circ\text{C}$ and $T_L = 40^\circ\text{C}$
- $P_s = 1.2\text{bar}$



Amine strength versus specific reboiler duty.



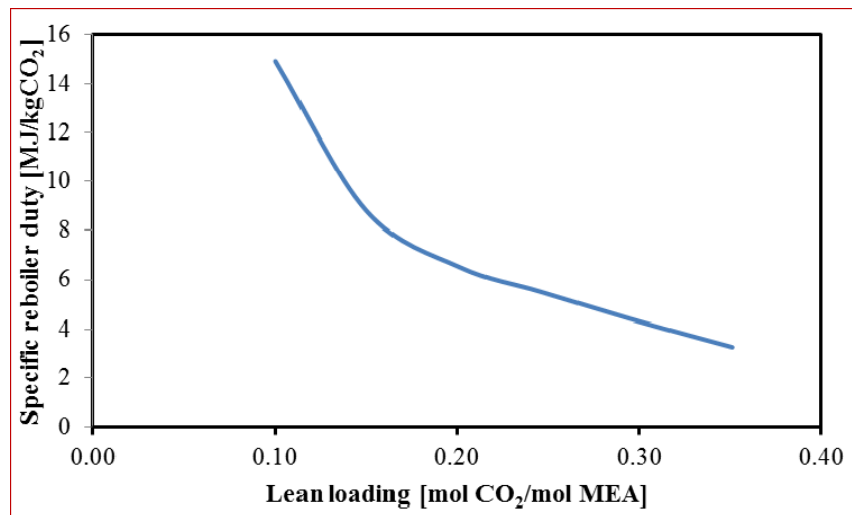
Absorber temperature profiles.



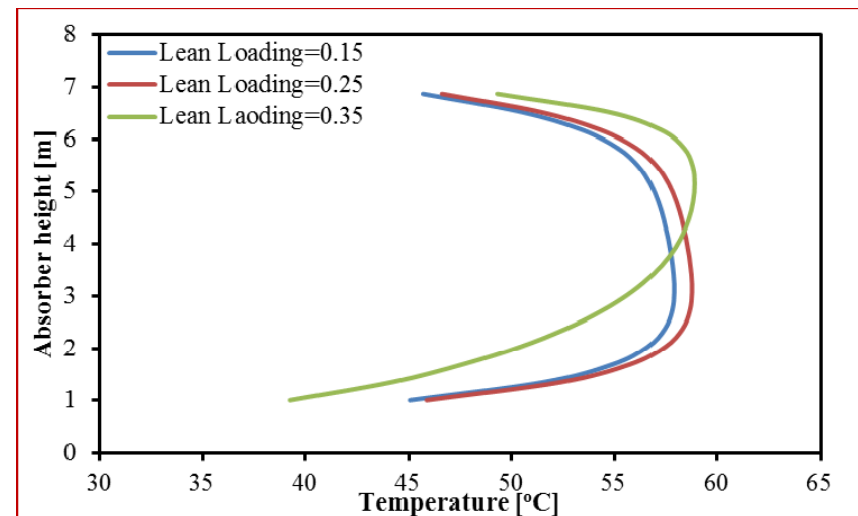
Set E: Variation of lean amine loading

Variation:

- $y_{\text{CO}_2} = 4.5\text{mol}\%$
- $L/G = 1.9$ and $\omega = 28.5\text{wt}\%$
- $0.10 \geq \alpha \geq 0.35$
- $\psi = 90\%$
- $T_G = 40^\circ\text{C}$ and $T_L = 40^\circ\text{C}$
- $P_s = 1.2\text{bar}$



Lean amine loading versus specific reboiler duty.



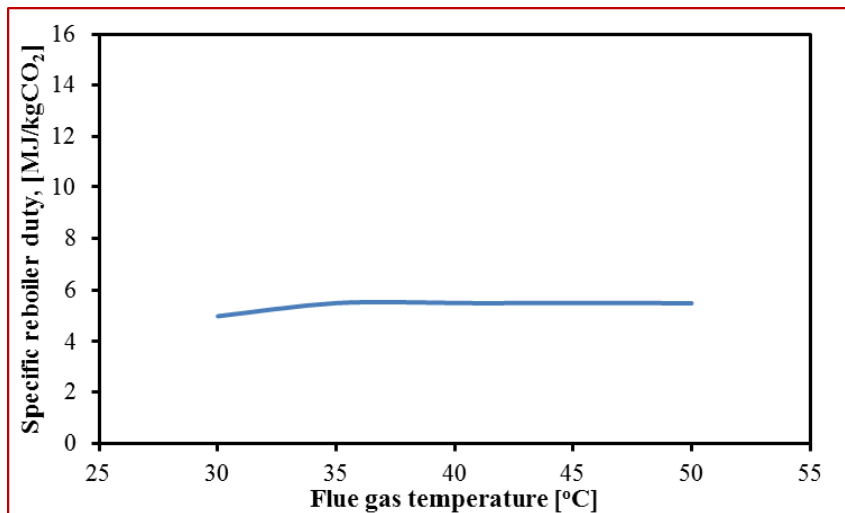
Absorber temperature profiles.



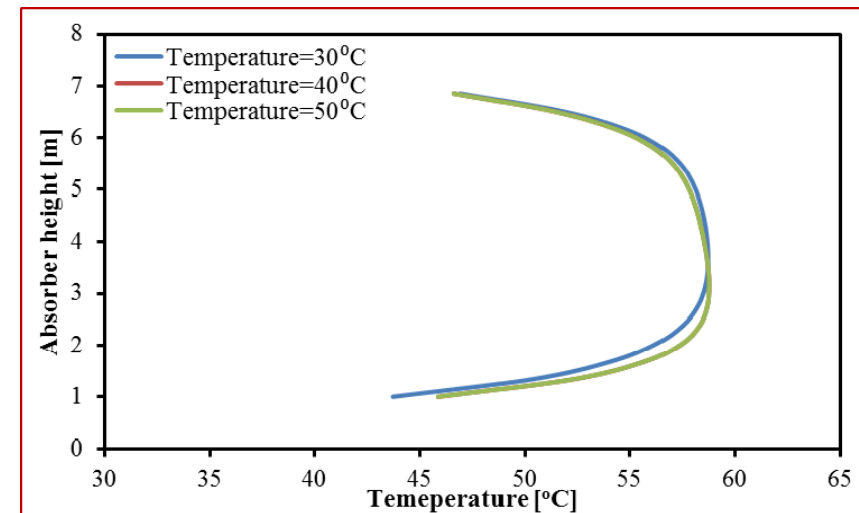
Set F: Variation of flue gas temperature

Variation:

- $y_{\text{CO}_2} = 4.5\text{mol}\%$
- $L/G = 1.9$ and $T_L = 40^\circ\text{C}$
- $\alpha = 0.25$ and $\omega = 28.5\text{wt}\%$
- $\psi = 90\%$
- $30^\circ\text{C} \geq T_G \geq 50^\circ\text{C}$
- $P_s = 1.2\text{bar}$



Flue gas temperature versus specific reboiler duty.



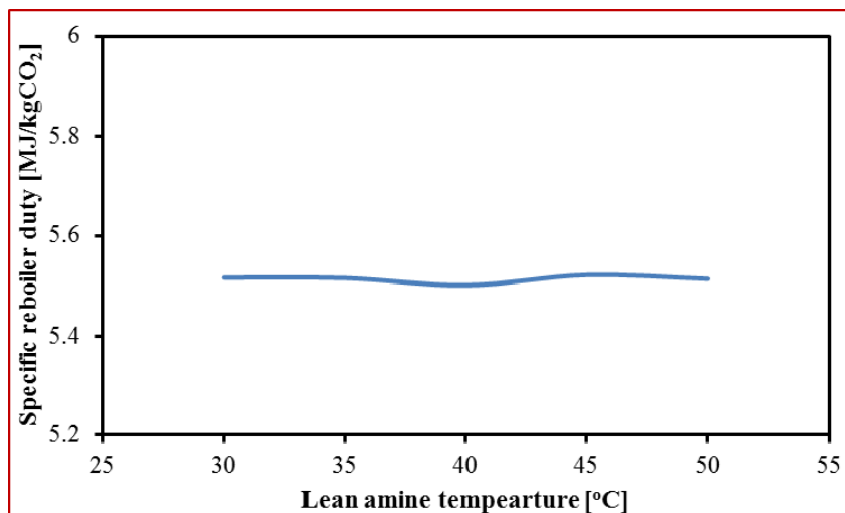
Absorber temperature profiles.



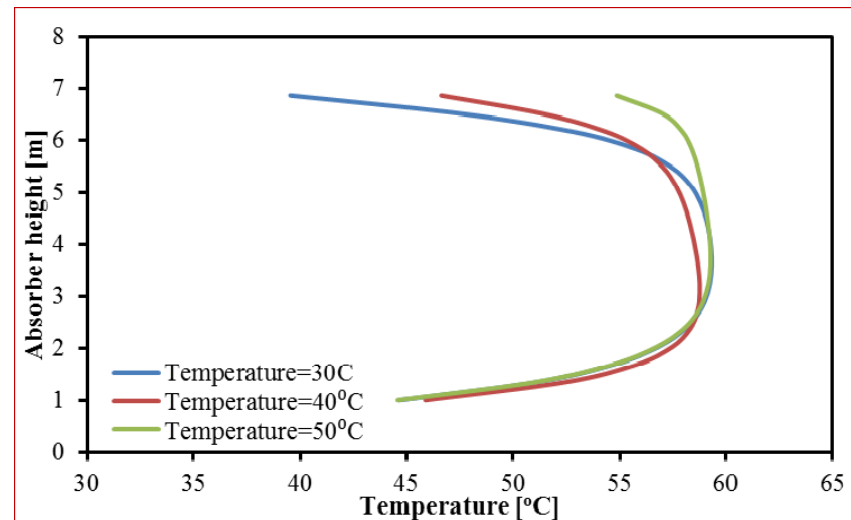
Set G: Variation of liquid temperature

Variation:

- $y_{\text{CO}_2} = 4.5\text{mol}\%$
- $L/G = 1.9$ and $T_G = 40^\circ\text{C}$
- $\alpha = 0.25$ and $\omega = 28.5\text{wt}\%$
- $\psi = 90\%$
- $30^\circ\text{C} \geq T_L \geq 50^\circ\text{C}$
- $P_s = 1.2\text{bar}$



Liquid temperature versus specific reboiler duty.



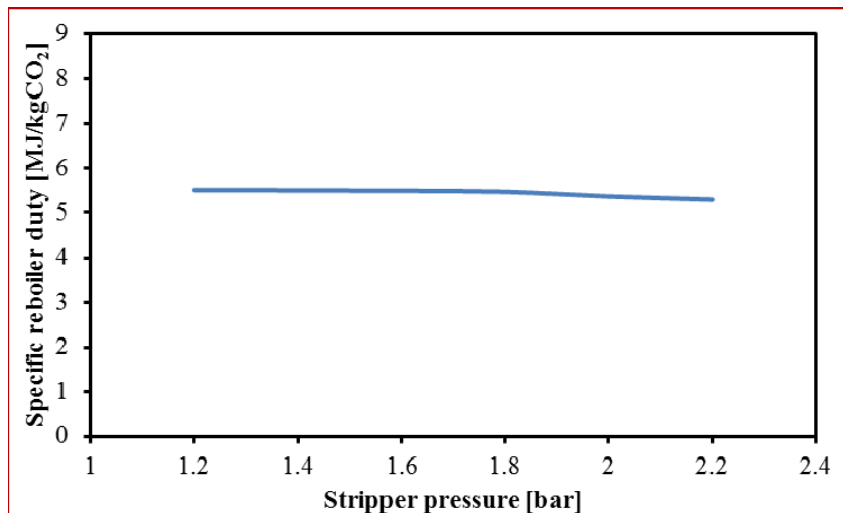
Absorber temperature profiles.



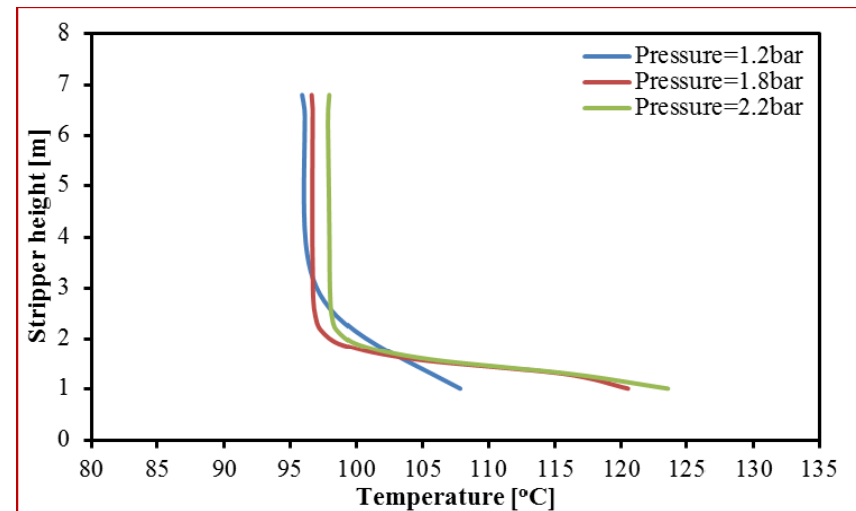
Set H: Variation of stripper pressure

Variation:

- $y_{\text{CO}_2} = 4.5\text{mol}\%$
- $L/G = 1.9$
- $\alpha = 0.25$ and $\omega = 28.5\text{wt}\%$
- $\psi = 90\%$
- $T_G = 40^\circ\text{C}$ and $T_L = 40^\circ\text{C}$
- $1.2\text{bar} \geq P_s \leq 2.2\text{bar}$



Stripper pressure versus specific reboiler duty.



Stripper temperature profiles.



Conclusions

- ❑ Process sensitivity analysis – a useful tool to analyse plant operability range.
- ❑ Higher CO₂ composition → decrease in the specific reboiler duty.
 - ~ 7.7% experimentally, 6.6% in the modelling.
- ❑ Higher CO₂ capture rate → higher specific reboiler duty.
- ❑ Optimum L/G ratio is about 1.0.
- ❑ The higher the amine strength, the lower is the specific reboiler duty.
- ❑ Lower lean amine loading → decreased cyclic capacity → reduced degree of regeneration.
- ❑ No comprehensive conclusion can be drawn for the temperatures.
- ❑ Higher stripper pressure → decreased specific reboiler duty → increased reboiler temperature.



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Thank you

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